

CHILlicothe ROAD
CHESTER TWP.

70

LEVEL BOOK

744

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PLEASE RETURN TO
 GAUGA COUNTY ENGINEER

COURT HOUSE
 CHARDON, O.
 PHONE 250-X

PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16.6 in.	21	3.46.6 in.	41	6.76.6 in.	61	10.06.6 in.	81	13.36.6 in.		
2	33.0	22	3.63.0	42	6.93.0	62	10.23.0	82	13.53.0		
3	49.6	23	3.79.6	43	7.09.6	63	10.39.6	83	13.69.6		
4	66.0	24	3.96.0	44	7.26.0	64	10.56.0	84	13.86.0		
5	82.6	25	4.12.6	45	7.42.6	65	10.72.6	85	14.02.6		
6	99.0	26	4.29.0	46	7.59.0	66	10.89.0	86	14.18.6		
7	1.15.6	27	4.45.6	47	7.75.6	67	11.05.6	87	14.35.6		
8	1.32.0	28	4.62.0	48	7.92.0	68	11.22.0	88	14.52.0		
9	1.48.6	29	4.78.6	49	8.08.6	69	11.38.6	89	15.08.6		
10	1.65.0	30	4.95.0	50	8.25.0	70	11.55.0	90	15.25.0		
11	1.81.6	31	5.11.6	51	8.41.6	71	11.71.6	91	15.41.6		
12	1.98.0	32	5.28.0	52	8.58.0	72	11.88.0	92	15.58.0		
13	2.14.6	33	5.44.6	53	8.74.6	73	12.04.6	93	16.14.6		
14	2.31.0	34	5.61.0	54	8.91.0	74	12.21.0	94	16.31.0		
15	2.47.6	35	5.77.6	55	9.07.6	75	12.37.6	95	16.47.6		
16	2.64.0	36	5.94.0	56	9.24.0	76	12.54.0	96	16.64.0		
17	2.80.6	37	6.10.6	57	9.40.6	77	12.70.6	97	16.80.6		
18	2.97.0	38	6.27.0	58	9.57.0	78	12.87.0	98	16.97.0		
19	3.13.6	39	6.43.6	59	9.73.6	79	13.03.6	99	17.13.6		
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	17.30.0		

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

CHILLICOTHE ROAD
 CHESTER TWP.

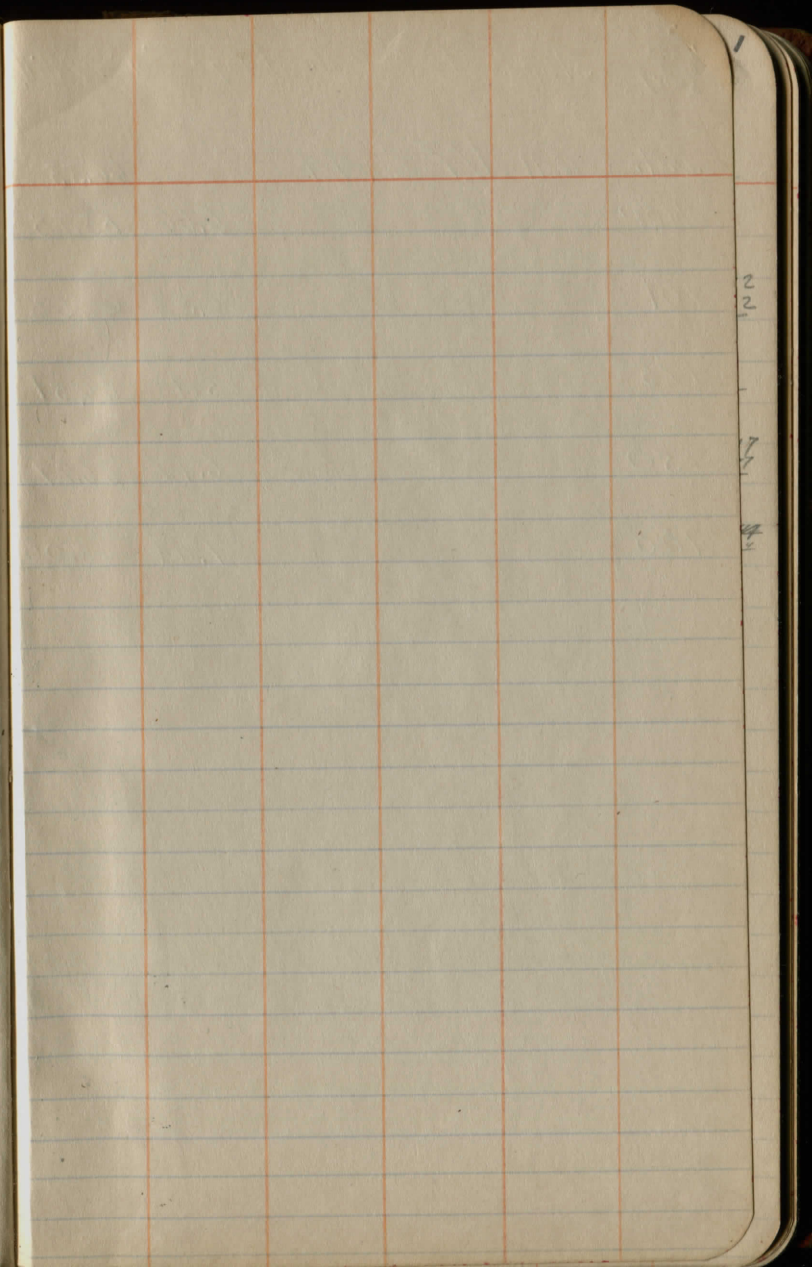
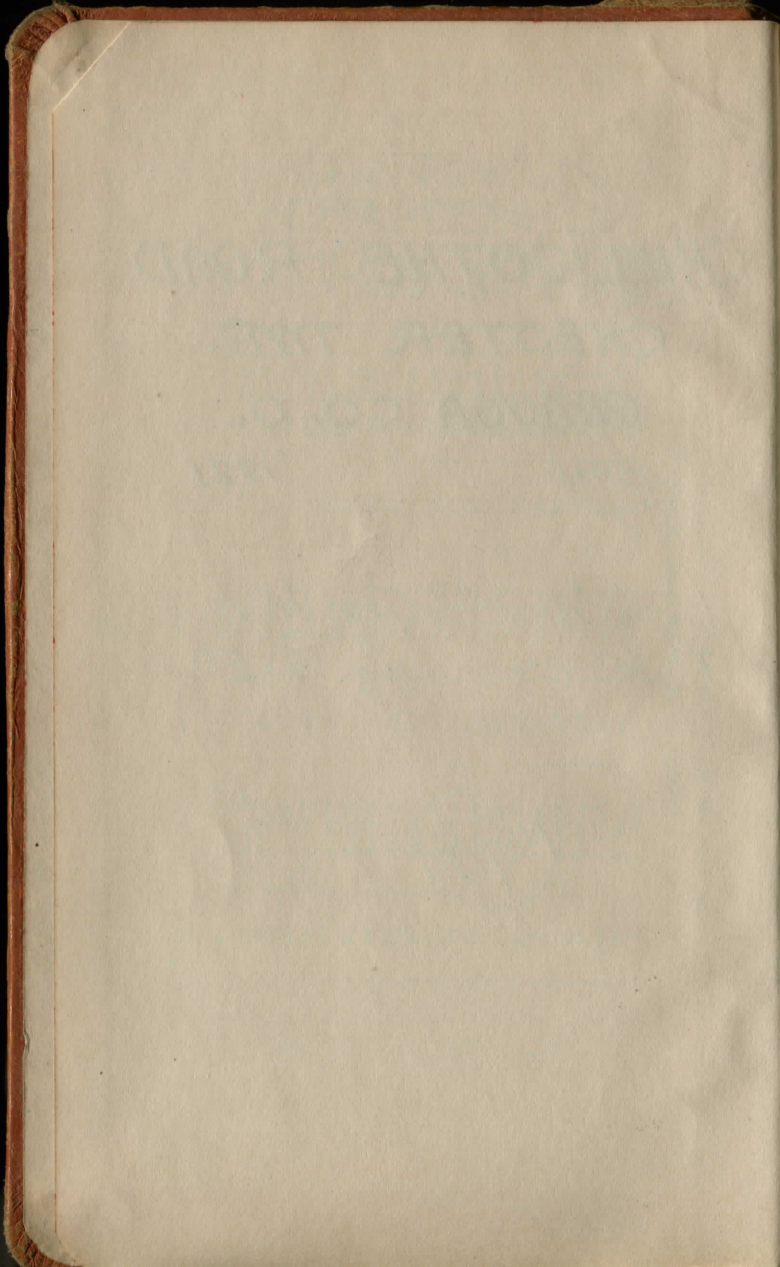
GAUGA CO., O..

B. R. Kenney
 Co. Surveyor.

1921

Benchmarks - pg. 1-7
 X-Sections - pg. 9-50

70



2-4-22
 Minno
 Gray
 sperry

Slopes for Grd. change Cominsory Hill.

J.M.	6.11	1272	44	66.33
101+50		6.66	65.78	
101		5.92	66.52	
+75		5.93	66.51	
+50		6.17	66.27	
100		7.44	65.00	

	Rt.		Lt.
$\frac{5.66}{5}$	$\boxed{C0.0}$	$\frac{6.00}{19.8}$	$\frac{F0.2}{19.5}$
			$\boxed{0.0}$
$\frac{5.92}{1.5}$	$\boxed{C1.5}$ Rt.	$\frac{C1.4}{21.9}$	$\frac{C1.1}{20.9}$
			$\boxed{C1.2}$ Lt.
$\frac{5.93}{1.4}$	Rt. $\boxed{C1.4}$	$\frac{C1.3}{21.7}$	$\frac{C1.5}{22.0}$
			$\boxed{C1.6}$ Lt.
$\frac{6.17}{1.2}$	Rt. $\boxed{C1.2}$		$\frac{C1.2}{21.5}$ Lt.
			$\boxed{C1.6}$ Lt.
$\frac{7.44}{0.5}$	Rt. $\boxed{C0.6}$	$\frac{C0.4}{20.4}$	$\frac{C1.7}{1.6}$
			$\frac{4.157}{1.6}$
		(Graded 3.3 But left of old point)	
			$\frac{7.44}{3.3}$

10-14-'21
Fair-Fine

BENCH

Sta. B.S. H. I. F.S. Elev.

B.M. 0.57 1217 45 1216.881

Temp. B.M. 5.16 1212.29

T.P. 5.53 1215 89 7.09 1210.36

B.M. 1.57 1214.32

T.P. 1.34 1215 01 2.22 1213.67

B.M. 8.23 1206.78

T.P. 7.75 1210 52 12.24 1202.77

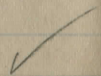
B.M. 3.30 1207.22

T.P. 0.95 1199 09 12.38 1198.14

T.P. 0.01 1187 01 12.09 1187.00

B.M. 8.87 1178.14

T.P. 0.66 1175.15 12.52 1174.49



MARKS

Hanna
Gard
Thompson

U.S.G.S. B.M., N.W. cor. Cottrell's store
Bronze tablet "1217 Cleveland.

x on S.W. cor S. Head Wall at X Roads.

Staple in N.W. root 18" Maple 74+60, 30' Rt.

Staple in W. root 24" Maple 30' Rt. Sta. 59+20

Staple in N.W. root 2nd Maple S. of D.W. Rt. 51+30

Staple in S.E. root 24" Maple 30' Lt. Sta 40+95

1175.15

T.P. 0.12 1162 28 12.99 1162.16

B.M. 3.17 1159.11 B.M. x on N.W. Cor. W. Head Wall Corn Culu. 33+85

T.P. 0.60 1149 94 12.94 1149.34

B.M. 9.61 1140.33 x on W. end N. Head Wall of Culu. over Rd to Rt.

T.P. 0.21 1137 47 12.68 1137.26

B.M. 7.24 1130.23 Staple in E root 24" Maple 30° Lt. Sta. 20+70

T.P. 8.91 1138 69 7.69 1129.78

T.P. 7.03 1141 30 4.42 1134.27

B.M. 4.12 1137.18 Staple in E. root, 20" Maple 30° Lt. Sta 1+45

T.P. 0.29 11 29 52 12.07 1129.23 Noon

T.P. 0.87 1117 81 12.58 1116.94

B.M. 9.31 1108.50 2nd step to Novelty Store
1108.70

✓

10-17-21

Fair-Breezy

B.M.s

North

Hanna
Grau
Thompson.

4

	(+) B.S.	H. I.		(-) F.S.	Elev.	
B.M.	5.60	1217	89		1212.29	x on S.E. Cor. S. Head Wall at X Rds.

T.P.	9.59	1227	29	0.19	1217.70	
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T.P.	7.81	1234	78	0.32	1226.97	
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B.M. →

T.P.	10.49	1245	02	4.29	1230.49	Staple in E. root 15" Maple 25' Lt. Sta 88+90
				0.25	1234.33	

T.P.	11.73	1256	30	0.45	1244.57	
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T.P.	11.96	1267	63	0.63	1255.67	
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T.P.	3.95	1271	33	0.25	1267.38	
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B.M.				5.00	1266.33	Staple in W. root 24" Elm, 35' Rt. Sta 102+18
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T.P.	0.31	1258	99	12.65	1258.68	
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T.P.	0.42	1248	68	10.73	1248.26	
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T.P.	1.80	1239	01	11.47	1237.21	
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B.M.				2.28	1236.73	Staple in W. root 10" Maple, 23' Rt. Sta 111+20
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✓

Sta.	B. S.	M. I.	F. S.	Elev.	
T.F.	2.72	1239.01 1230.49	11.24	1227.77	
T.F.	0.42	1218.58	12.33	1218.16	
B.M.			7.67	1210.91	Staple in W. root 12" Maple, 26 Rt. Sta. 125+14
T.F.	0.38	1207.61	11.35	1207.23	
B.M.	0.68	1197.34	10.95	1196.66	Staple in W. Root 30" Elm 30' Rt. Sta. 131+80
T.F.	3.19	1190.85	9.68	1187.66	
B.M.			3.50	1187.35	Staple in S.E. root 18" Locust 30' Lt. Sta. 144+60
T.F.	0.61	1179.76	11.70	1179.15	
T.F.	8.40	1177.75	10.41	1169.35	
B.M.			3.02	1174.73	Staple in N.W. root 14" Maple, 25' Rt. Sta. 162+10
T.F.	0.41	1166.80	11.36	1166.39	
T.F.	10.27	1172.02	5.05	1161.75	
T.F.	8.34	1176.43	3.93	1168.09	

1176 43

B.M. 3.62 1172.81 Staple in S.E. root 24" P. Hickory, 30' Lt 183+40

T.P. 0.22 1165 06 11.59 1164.84

T.P. 0.82 1153 82 12.06 1153.00

B.M. 2.29 1151.53 Staple in N.W. root 12" Walnut 30' Rt. Sta. 197

T.P. 0.89 1141 81 12.90 1140.92

T.P. 0.30 1140 49 1.62 1140.19 S.E. Cor. Con. porch floor to store

Noon

B.M. 5.71 1134.78 Staple in S.E. root 10" Maple 30' Lt. 206+27

T.P. 9.47 1144 83 5.13 1135.36

T.P. 4.16 1141 71 7.28 1137.55

B.M. 2.07 1139.64 Staple in N.W. root 12" Maple 30' Rt. 215+85

T.P. 0.79 1129 91 12.59 1129.12

T.P. 0.49 1118 17 12.23 1117.68

T.P. 0.20 1105 88 12.49 1105.68

✓

110588

T.F. 423 1098 04 12.07 1093.81

B.M. 1.92 1096.12

7
staple in E. root 12" ^{Elm}Maple, 85' Lt 225+75
Maple o.k.

T.F. 1.21 1089 60 9.65 1088.39

T.F. 1.74 1083 68 7.66 1081.94

B.M. 3.27 1080.41

Staple S.E. root 12" W. Cherry, 30' Rt., 240+10

T.F. 5.61 1081 76 7.53 1076.15

T.F. 6.18 1077 53 10.41 1071.35

B.M. 3.97 1073.56

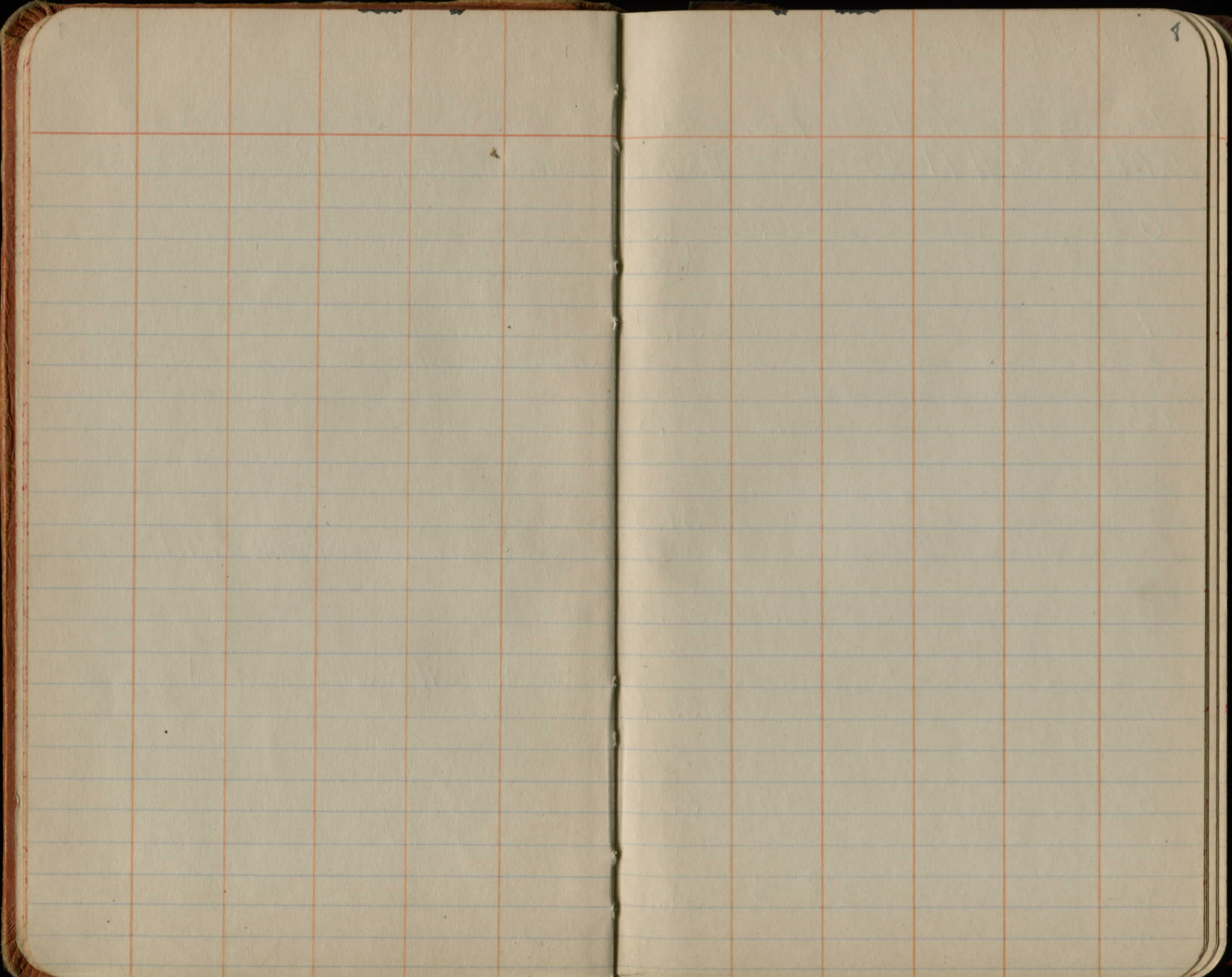
Staple S.W. root, 14" Maple 27' Rt., 252+90

T.F. 9.90 1084 65 2.78 1074.75

B.M. +0.10 1084.75

Spike in S.W. side 12" Apple 60' Lt. on Co line





10-14-'21 P.M.
Fair-Fine

CROSS -

Sta.	B.S.	H.I.	F.S.	Elev.
B.M.	4.09	1141	27	1137.18
0		✓	10.0	31.3
1		-	6.4	34.9
+75			7.5	36.8
2		-	4.3	37.0
3		-	4.5	36.8
4		-	5.6	35.7
5		-	6.5	34.8
6		-	6.3	35.0

SECTIONS

Hanna
Gred
Thompson

Lt & Rt

Staple in E. root 20" Maple 30" Lt. staple

+2.0	+0.5	0.0	-1.5	-0.6	0.0	0.0	-0.8	+0.5	+2.2	+2.8
8.0	9.5	10.0	11.5	10.6	10.0	10.0	10.8	9.5	7.8	7.2
25	21	17	13	11	8	4	9	13	20	25

ends of

+1.1	+0.7	-1.0	-0.4	0.0	-0.1	-0.9	+1.7	+3.6
5.3	5.7	7.4	6.8	6.4	6.5	7.3	4.7	2.8
25	14	12	8	4	9	13	25	

0.0	-0.1	-0.9	-0.5	0.0	-0.3	-0.8	+2.0	+3.8
1.5	1.6	5.4	5.0	1.5	4.8	5.3	2.5	0.1
25	16	14	10	4	9	13	25	

-0.4	-0.8	0.0	0.0	-0.3	-0.8	+1.8	+2.5	+3.5
4.7	5.1	4.3	4.3	4.6	5.1	2.5	1.8	0.8
2.5	14	2	4.3	5	8	13	21	2.5

-0.5	-0.1	-0.8	0.0	0.0	-0.2	-0.6	+1.0	+1.9	+2.3	+3.8
5.9	4.6	5.3	4.5	4.5	4.7	5.1	3.5	2.6	2.2	0.7
25	12	13	3	4.5	4	8	10	13	17	25

-0.7	-0.3	-1.0	0.0	0.0	-1.0	+0.7	+1.9	+2.6
6.3	5.9	4.6	5.6	5.6	6.6	4.9	3.7	3.0
2.5	15	13	3	5.6	7	10	7.8	2.5

-1.4	-0.5	-0.9	-0.5	0.0	0.0	-0.3	-0.9	+0.3	-0.1	+0.6	+1.5
7.4	7.0	7.4	7.0	6.5	6.5	6.3	7.4	6.2	6.6	5.9	5.0
2.5	16	14	12	4	6.5	4	7	9	15	21	2.5

-1.7	-1.0	-1.7	-0.6	+0.1	0.0	-0.2	-1.0	-0.3
8.0	7.3	8.0	6.9	6.2	6.3	6.5	7.3	6.6
2.5	14	13	10	4	6.3	3	7-17	2.5

Sta. B.S. H. I. F.S. Elev.
 1141 27
 5+92 = 12" C.I.P.
 T.P. 3.46 1138 29 6.44 1134.83

7 - 3.7 34.6

8 - 5.6 32.7

9 - 7.5 30.8

10 - 8.3 30.0

+35 = 12" C.I.P. sec. 8.1 30.2

11 - 8.3 30.0

T.P. 8.27 1138 24 8.32 1129.97

10

-1.8 -1.2 1.7 -1.9 -0.4 0.0 -0.4 -1.5 -1.0 -0.7 -0.3
 $\frac{7.9}{25}$ $\frac{7.3}{17}$ $\frac{7.8}{14}$ $\frac{7.565}{11}$ $\frac{6.1}{9}$ $\frac{6.5}{5}$ $\frac{7.5}{2}$ $\frac{7.1}{8}$ $\frac{6.8}{15}$ $\frac{6.9}{25}$

← 12" C.I.P. sectional
 Good Cond. filled with \leftarrow 16' \rightarrow

-1.4 -0.9 -1.8 -0.5 +0.1 0.0 -0.1 +0.5 +0.9
 $\frac{5.1}{25}$ $\frac{4.6}{15}$ $\frac{5.5}{14}$ $\frac{4.2}{10}$ $\frac{3.6}{4}$ $\frac{3.7}{4}$ $\frac{3.8}{8}$ $\frac{3.7}{10}$ $\frac{2.8}{25}$

+0.2 -0.4 -1.7 -0.2 +0.1 0.0 -0.8 +1.7 +2.2 +2.6
 $\frac{5.4}{25}$ $\frac{4.0}{15}$ $\frac{7.3}{14}$ $\frac{5.8}{8}$ $\frac{5.5}{5}$ $\frac{5.6}{5}$ $\frac{6.4}{7}$ $\frac{3.9}{11}$ $\frac{3.4}{16}$ $\frac{3.0}{25}$

+0.1 -0.4 -1.1 -0.3 +0.1 0.0 -1.0 -0.2 +1.1 +1.8
 $\frac{7.4}{25}$ $\frac{7.4}{15}$ $\frac{8.4}{14}$ $\frac{7.8}{9}$ $\frac{7.4}{5}$ $\frac{7.5}{5}$ $\frac{8.5}{6.7}$ $\frac{7.7}{8}$ $\frac{6.4}{13}$ $\frac{5.7}{25}$

-1.9 -0.8 -1.2 -0.6 -0.1 0.0 -0.2 -1.3 -0.3 0.0
 $\frac{10.2}{25}$ $\frac{9.1}{16}$ $\frac{9.5}{15}$ $\frac{8.9}{12}$ $\frac{8.4}{5}$ $\frac{8.3}{5}$ $\frac{8.5}{4}$ $\frac{9.6}{7.8}$ $\frac{8.6}{10}$ $\frac{8.3}{25}$

-4.3 -3.5 -3.0 -0.6 0.0 0.0 -0.2 -2.4 -1.4 -0.7
 $\frac{12.4}{50}$ $\frac{11.6}{25}$ $\frac{11.1}{19}$ $\frac{8.7}{13}$ $\frac{8.1}{2}$ $\frac{8.1}{2}$ $\frac{8.3}{3}$ $\frac{10.5}{4.5}$ $\frac{9.5}{11}$ $\frac{8.8}{16}$

← 16' \rightarrow
 Good Cond.

-1.1 -1.2 -0.6 -0.8 +0.1 0.0 -0.4 -1.0 -0.1 +0.5
 $\frac{8.4}{25}$ $\frac{8.5}{20}$ $\frac{8.9}{15}$ $\frac{9.1}{14}$ $\frac{8.2}{6}$ $\frac{8.3}{6}$ $\frac{8.7}{3}$ $\frac{9.3}{5}$ $\frac{8.4}{9}$ $\frac{7.5}{25}$

1138 24

12 - 7.6 30.6

13 - 5.9 32.3

14 - 4.8 33.4

15 - 3.9 34.3

16 - 3.9 34.3

+60 - 4.4 33.8

17 - 5.6 32.6

18 - 8.0 30.2

T.P. 4.17 1134 06 8.35 1129.89

$$\begin{array}{cccccccc}
 0.0 & +0.1 & -0.6 & +0.3 & 0.0 & -1.0 & +0.3 & +1.6 & +2.3 \\
 0.7 & 7.5 & 25 & 8.2 & 7.3 & 7.6 & 8.6 & 7.3 & 6.0 & 5.3 \\
 25 & 14 & 13 & 4 & & & 6 & 8 & 12 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 -0.5 & -0.1 & -0.8 & +0.2 & 0.0 & -0.2 & -1.0 & -0.4 & +0.5 & +1.4 \\
 6.4 & 6.0 & 6.7 & 5.7 & 5.9 & 6.1 & 6.9 & 6.3 & 5.4 & 4.5 \\
 25 & 13 & 12 & 4 & & 2 & 6.7 & 8 & 12 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 -1.0 & -0.6 & -1.1 & 0.0 & 0.0 & -1.4 & +0.7 & +1.4 & +1.7 \\
 5.8 & 5.4 & 5.9 & 4.8 & 4.8 & 6.2 & 4.1 & 3.4 & 3.1 \\
 25 & 13 & 12 & 3 & & 8 & 12 & 14 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 -1.3 & -0.7 & -1.3 & 0.0 & 0.0 & -0.4 & -1.2 & +1.5 & +2.0 \\
 5.2 & 4.6 & 5.2 & 3.9 & 3.9 & 4.3 & 5.1 & 2.4 & 1.9 \\
 25 & 13 & 12 & 4 & & 8 & 9 & 13 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 -0.5 & -0.2 & -1.2 & +0.1 & 0.0 & -0.5 & -1.3 & +1.3 & +1.5 \\
 4.4 & 4.1 & 5.1 & 3.8 & 3.8 & 4.4 & 5.2 & 2.6 & 2.4 \\
 25 & 14 & 12 & 3 & & 5 & 10 & 14 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 +0.2 & +0.3 & -1.5 & -0.5 & 0.0 & -0.4 & -1.4 & +1.2 & +2.0 \\
 4.2 & 4.1 & 5.7 & 4.7 & 4.4 & 4.8 & 5.8 & 3.2 & 2.4 \\
 25 & 14 & 12 & 8 & & 4 & 9 & 13 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 +0.8 & +0.9 & -1.4 & -0.2 & 0.0 & -0.3 & -1.5 & +1.6 & +2.8 \\
 4.8 & 4.7 & 7.0 & 5.8 & 5.6 & 5.9 & 7.1 & 4.0 & 2.8 \\
 25 & 14 & 12 & 4 & & 4 & 9 & 14 & 2.5
 \end{array}$$

$$\begin{array}{cccccccc}
 +0.7 & 0.0 & +0.1 & -1.1 & -0.4 & 0.0 & -0.2 & -1.2 & 0.0 & +1.5 & +2.0 \\
 7.3 & 8.0 & 7.9 & 9.1 & 8.4 & 8.0 & 8.3 & 9.2 & 8.0 & 6.8 & 6.0 \\
 25 & 20 & 13 & 12 & 7 & & 4 & 10 & 12 & 13 & 2.5
 \end{array}$$

✓

✓

113406

12 19 - 4.3 29.8

13 20 - 4.5 29.6

14 +75 - 5.1 29.0
diff of 0.07

15 21 B.M. 3.90 1134.13 3.90 ^{30.23} 1130.16 - 5.8 28.3

16 22 - 8.3 25.8

+6 Temp B.M. 8.89 1136.11 6.91 1127.22

22 +95 2 1/2 x 2 1/2 Stone Box 10.2 25.9

17

18 23 - 10.2 25.9

Ti

-1.1 -0.8 -1.6 -0.7 0.0 -0.3 -1.6 -0.3 0.0
5.4 5.1 5.7 5.0 4.3 4.4 5.7 4.6 4.3
2.5 1.3 1.1 0.8 1.0 1.1 1.1 1.3 2.5

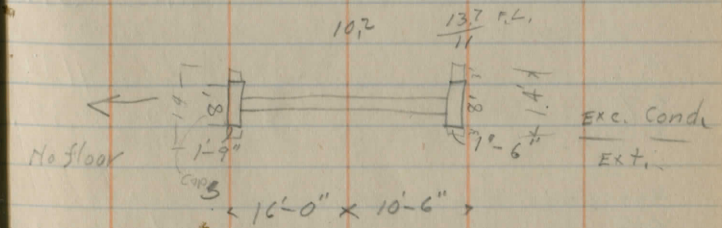
-0.3 -1.0 -1.7 -0.5 -0.1 0.0 -0.2 -0.9 -0.4 -0.1
4.8 5.5 6.2 5.0 4.4 4.5 4.7 5.4 4.9 4.6
2.5 1.4 1.3 0.9 0.4 0.4 1.1 1.4 2.5

+0.6 -0.6 -2.1 -0.9 +0.3 0.0 -0.5 -2.2 -1.1 0.0 +0.4
4.5 5.7 7.2 6.0 4.8 5.1 5.6 7.3 6.2 5.1 4.7
2.5 1.6 1.5 1.1 0.4 0.6 1.0 1.1 1.2 1.5 2.5

E. root 24" Maple 30' Lt. Sta 20+70
^{30.23}
+0.6 -0.6 -2.1 -0.5 +0.2 0.0 -0.6 -2.4 +0.7 +1.1
5.2 6.4 7.2 6.3 5.2 5.8 6.4 8.2 5.1 4.7
2.5 1.7 1.5 1.4 1.0 0.5 0.5 0.9 1.0 1.5 2.5

+0.4 -0.3 -1.1 -0.1 0.0 -0.2 -1.4 -0.4 +1.7 +2.6
7.9 8.4 9.7 8.4 8.3 8.5 9.7 8.7 6.4 5.7
2.5 2.0 1.7 1.5 1.5 1.0 0.9 1.0 1.2 1.6 2.5

x S.E. Cor. W. parapet.



-1.9 -1.5 -2.5 -0.5 +0.2 0.0 +0.1 -1.5 -3.3 -1.8 -2.3
12.1 11.7 12.7 10.7 10.0 10.2 10.1 11.7 13.5 12.0 12.5
2.5 2.0 1.4 1.8 1.6 0.6 1.0 1.4 1.5 1.6 1.8 2.5

1136 11

24 - 9.3 26.8

-0.4 -1.1 -0.6 -0.1 0.0 -0.5 -2.0 +0.2 +0.4
91 10.4 99 94 93 98 113 91 89
25-18 17-16 14 7 11 14-15 17 25

25 - 7.1 29.0

+2.1 -0.6 -1.6 -0.7 +0.1 0.0 -0.4 -2.0 +0.5 +1.1
50 77 87 78 70 71 75 91 66 60
25-23 20-19 17-17 14-11 3 9 13-14 20 25

26 - 2.7 33.4

+1.6 -0.3 -0.1 0.0 -0.3 -1.3 +0.8 +1.6
11 3.9 28 27 3.0 5.0 1.9 11
25 12 13 11 15-17 21 25
Tilt in Lt. ditch

T.P. 961 1145 16 0.5C 1135.55

+70 - 7.1 38.1

-0.4 -0.5 +0.2 -0.2 0.0 +0.6 -2.1
75 76 69 73 71 65 92
25 17 11 3 19 25 at sand culv.

+77- & Rd. 6.7 38.5

& E & W Rd.

4.6 40.6

25' Rt. top culv.

4.5 40.7

50' Rt.

6.8 38.4

25' Lt.

7.9 37.2

50' Lt.

B.M. 384 1140.32

Take Lt. Ditch water W. along W. road ditch

27 - 5.5 39.7

x on N. Head Wall
72 -1.7 -0.7 0.0 +0.5 -3.3
30 25 5.5 5.0 8.8
19 25

28 - 3.7 41.5

-1.1 -0.4 -1.4 -0.6 0.0 -0.5 -2.2 -0.5 +0.2
43 41 51 43 37 43 50 42 3.5
25 15 13-11 9 10 14-16 18-23 25

29 - 1.4 43.8

-1.6 -0.7 -1.5 -0.5 0.0 -0.5 -1.2 -0.6 -0.2
30 21 29 19 14 19 26 20 16
25 13 11 8 8 11-12 14 25

T.P. 989 1154 59 0.46 1144.70

1154.59

30 - 81 46.5

31 - 38 50.8

T.P. 824 1161 37 1.46 1153.13

32 - 5.1 56.3

+55 4.0 57.4

33 - 4.5 56.9

+80 3x2 1/2 Con Box 3.7 57.7

34 - 39 57.5

35 - 33 58.1

BM, 2.28 1154.09

14

+1.6 +1.3 +0.1 -1.2 -0.1 0.0 -0.3 -1.3 -0.4 -0.1 +0.7
 $\frac{6.5}{25} \frac{6.8}{20} \frac{8.0}{14} \frac{9.3}{12-10} \frac{8.2}{4} \frac{8.1}{7} \frac{8.4}{10-11} \frac{9.4}{12} \frac{8.5}{21} \frac{8.7}{25}$

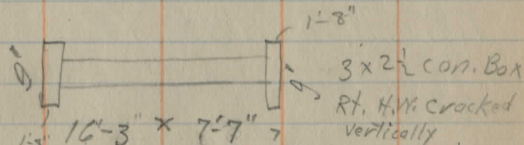
-0.1 0.0 -0.8 -0.1 +0.1 0.0 -0.1 -1.2 +1.4 +1.8 +2.6 +3.2
 $\frac{3.7}{25} \frac{3.8}{12} \frac{4.6}{13} \frac{3.9}{9} \frac{3.7}{4} \frac{3.8}{7} \frac{3.9}{1} \frac{5.0}{9-10} \frac{2.4}{13} \frac{2.0}{16} \frac{1.2}{20} \frac{0.6}{25}$

-0.8 -0.7 -1.2 -0.2 +0.2 0.0 +0.1 +1.7 +2.6
 $\frac{5.9}{25} \frac{5.8}{17} \frac{6.3}{15} \frac{5.3}{9} \frac{4.9}{4} \frac{5.1}{7} \frac{5.0}{9} \frac{3.4}{14} \frac{2.5}{25}$

-1.3 -1.3 -1.7 -0.1 +0.1 0.0 -0.7 -0.2 +1.7
 $\frac{5.3}{25} \frac{5.3}{17} \frac{5.7}{15} \frac{4.1}{9} \frac{3.9}{5} \frac{4.0}{7} \frac{4.7}{8} \frac{4.2}{10-13} \frac{2.1}{25}$

-0.7 -1.2 -1.3 -0.2 +0.3 0.0 -0.1 -1.1 +0.1 +1.3 +2.9
 $\frac{5.2}{25} \frac{5.7}{23-17} \frac{5.8}{15} \frac{4.7}{11} \frac{4.2}{6} \frac{4.5}{7} \frac{4.6}{3} \frac{5.6}{7-8} \frac{4.4}{11} \frac{3.2}{18} \frac{1.5}{25}$

0.0 -3.6 -1.4 -0.5 +2.4
 $\frac{3.7}{0-8} \frac{7.3}{8} \frac{5.1}{14} \frac{4.7}{18} \frac{1.3}{25}$



1'-16-3\" x 7'-7\"
 -2.3 -3.0 -1.9 -0.2 +0.3 0.0 -0.1 -2.1 -2.9 -1.2 -1.8 +1.7
 $\frac{6.2}{25} \frac{6.9}{23} \frac{5.3}{19} \frac{4.1}{11} \frac{3.6}{6} \frac{3.9}{7} \frac{4.0}{6} \frac{6.0}{11} \frac{6.3}{12-13} \frac{5.1}{15} \frac{5.0}{19} \frac{2.5}{25}$

-1.2 -0.9 -1.3 -0.5 0.0 0.0 -0.3 -1.6 -0.3 -0.6 -0.1
 $\frac{4.5}{25} \frac{4.2}{17} \frac{4.6}{16} \frac{3.3}{11} \frac{3.3}{4} \frac{3.3}{7} \frac{3.6}{5} \frac{4.9}{9-10} \frac{3.5}{11} \frac{3.9}{19} \frac{3.7}{25}$

X on N.W. Cor W. Head Wall Con. July, 33+85

10-15-'21
Fair-Finer

Sta B.S. H. I. F.S. Elev

B.M. 10.05 1169^r 16 1159.11

36 - 9.7 59.5

37 - 7.4 61.8

38 - 3.8 65.4

T.F. 10.06 1178 94 0.28 1168.88

39 - 10.7 68.2

40 - 8.0 70.9

B.M. 0.79 1178.15

41 - 3.8 75.1

T.F. 11.68 1189 79 0.83 1178.11

42 - 11.5 78.3

43 - 9.0 80.8

44 - 6.0 83.8

Hanna
Grau
Thompson

Lt. E. Rt.

-0.5 -0.1 -1.1 0.0 0.0 -0.5 -1.4 -0.1 +1.3+2.4+3.9
 $\frac{10.2}{2.5} \frac{9.8}{15} \frac{10.3}{13} \frac{9.7}{7} \frac{9.7}{5} \frac{10.2}{5} \frac{11.1}{9} \frac{9.8}{12} \frac{9.4}{16} \frac{7.3}{23} \frac{5.8}{25}$

+1.4 +1.0 -1.1 -0.5 +0.1 0.0 0.0 -0.7 -0.3 +3.9 +3.6
 $\frac{6.0}{2.5} \frac{6.4}{12} \frac{8.5}{13} \frac{7.9}{10} \frac{7.3}{5} \frac{7.4}{5} \frac{8.1}{9} \frac{7.7}{11} \frac{3.5}{19} \frac{3.8}{25}$

+0.8 +0.9 -1.0 -0.5 +0.2 0.0 +0.1 -1.3 -1.0 +2.4 +2.3
 $\frac{3.0}{2.5} \frac{2.9}{15} \frac{4.8}{12} \frac{4.3}{10} \frac{3.6}{5} \frac{3.8}{6} \frac{3.7}{9} \frac{5.1}{10} \frac{4.8}{12} \frac{1.4}{15} \frac{1.5}{25}$

+1.8 +0.8 +0.1 -1.2 -0.3 +0.2 0.0 -0.2 -1.1 -0.8 +0.7 +1.3
 $\frac{8.9}{2.5} \frac{9.9}{22} \frac{10.5}{14} \frac{11.9}{12} \frac{11.0}{9} \frac{10.5}{4} \frac{10.7}{7} \frac{10.9}{7} \frac{11.3}{10} \frac{11.5}{13} \frac{10.0}{16} \frac{9.4}{25}$

+2.3 +1.7 +0.8 -1.0 -0.2 +0.2 0.0 -0.3 -1.0 +1.4 +2.5
 $\frac{5.7}{2.5} \frac{6.3}{17} \frac{7.2}{14} \frac{9.0}{12} \frac{8.2}{7} \frac{7.8}{3} \frac{8.0}{5} \frac{8.3}{9} \frac{9.0}{11} \frac{6.6}{14} \frac{5.5}{18} \frac{5.5}{25}$

Staple in S.E. root 24" Maple 30' Lt. Sta 40+95

+2.2 +1.0 -2.2 -0.2 +0.2 0.0 -0.3 -1.3 +1.2 +2.1
 $\frac{1.6}{2.5} \frac{2.8}{15} \frac{6.0}{11} \frac{4.0}{8} \frac{3.6}{3} \frac{3.8}{5} \frac{4.1}{8} \frac{5.1}{10} \frac{2.6}{12} \frac{1.7}{15} \frac{1.7}{25}$

+1.5 +0.6 -1.5 -0.4 +0.1 0.0 -0.1 -1.4 +0.7 +1.2
 $\frac{10.0}{2.5} \frac{10.9}{15} \frac{13.0}{12} \frac{11.9}{9} \frac{11.4}{2} \frac{11.5}{5} \frac{11.6}{8} \frac{13.9}{11} \frac{10.8}{14} \frac{10.3}{25}$

+1.0 +0.1 -1.1 -0.2 +0.2 0.0 -0.2 -1.2 +0.4 +1.2
 $\frac{8.0}{2.5} \frac{8.9}{15} \frac{10.1}{13} \frac{9.2}{9} \frac{8.8}{3} \frac{9.0}{5} \frac{9.2}{7} \frac{10.2}{11} \frac{8.6}{13} \frac{7.8}{15} \frac{7.8}{25}$

+0.4 -0.4 -1.6 -0.6 0.0 0.0 -0.4 -1.7 +0.1 +1.3
 $\frac{5.6}{2.5} \frac{6.4}{15} \frac{7.6}{13} \frac{6.6}{9} \frac{6.0}{4} \frac{6.0}{4} \frac{6.4}{6} \frac{7.7}{10} \frac{5.9}{11} \frac{4.7}{14} \frac{4.7}{25}$

1189 79

45 ∞ 4.0 85.8

46
T.F. 12.77 1201 76 1.8 88.0
0.80 1188.99

47 - 11.0 90.8

48 - 8.4 93.4

49 - 5.4 96.4

50
T.F. 7.13 1208 61 2.0 99.8
0.28 1201.48

51 - 5.1 1203.5

B.M. 1.35 12 07.22

52 - 1.7 06.9

+50 ✓ - 0.7 07.9 ✓

+0.5 +0.2 -1.1 -0.5 -0.1 0.0 -0.6 -1.6 +0.1 +1.3 +2.3
 $\frac{3.5}{25}$ $\frac{3.8}{16}$ $\frac{5.1}{14-13}$ $\frac{4.5}{10}$ $\frac{4.1}{4}$ $\frac{4.0}{7}$ $\frac{4.6}{21.0}$ $\frac{5.6}{71}$ $\frac{3.9}{15}$ $\frac{2.7}{2.5}$

-0.3 0.0 -1.0 -0.1 +0.2 0.0 +0.3 -0.7 +0.4 +1.0
 $\frac{2.1}{25}$ $\frac{1.8}{77}$ $\frac{2.8}{15}$ $\frac{1.9}{12}$ $\frac{1.6}{2}$ $\frac{1.8}{8}$ $\frac{1.5}{10}$ $\frac{2.5}{12}$ $\frac{1.4}{12}$ $\frac{0.8}{2.5}$

-0.9 -0.6 -1.4 -0.5 +0.2 0.0 -0.1 -1.1 -0.4 +0.5
 $\frac{11.9}{25}$ $\frac{11.6}{17}$ $\frac{12.4}{14-15}$ $\frac{11.5}{12}$ $\frac{10.8}{5}$ $\frac{11.0}{5}$ $\frac{11.1}{5}$ $\frac{12.1}{9}$ $\frac{11.4}{12}$ $\frac{10.5}{2.5}$

-0.2 -0.4 -1.6 -0.6 +0.3 0.0 -0.5 -1.4 -0.8 -0.3 +1.4
 $\frac{8.6}{25}$ $\frac{8.8}{17}$ $\frac{10.0}{15}$ $\frac{9.0}{12}$ $\frac{8.1}{3}$ $\frac{8.4}{5}$ $\frac{8.9}{5}$ $\frac{9.8}{8}$ $\frac{9.2}{10}$ $\frac{8.7}{11}$ $\frac{7.0}{2.5}$

+1.1 +0.5 -1.4 -0.6 +0.3 0.0 -0.2 -1.1 +0.9 +1.9
 $\frac{4.3}{25}$ $\frac{4.9}{20}$ $\frac{6.8}{12-15}$ $\frac{6.0}{13}$ $\frac{5.1}{5}$ $\frac{5.4}{5}$ $\frac{5.6}{6}$ $\frac{6.5}{9-10}$ $\frac{4.5}{14}$ $\frac{3.5}{2.5}$

+1.0 +0.7 -1.4 -0.1 +0.3 0.0 +0.2 -0.2 +0.9 +1.4
 $\frac{1.0}{25}$ $\frac{1.3}{19}$ $\frac{3.4}{15}$ $\frac{2.1}{14}$ $\frac{1.7}{9}$ $\frac{2.0}{5}$ $\frac{1.8}{8}$ $\frac{2.7}{10}$ $\frac{1.1}{12}$ $\frac{0.9}{2.5}$

-0.2 -0.8 -1.5 -0.7 +0.1 0.0 -0.6 -1.5 +0.3 +1.6
 $\frac{5.2}{25-16}$ $\frac{5.9}{13}$ $\frac{6.6}{12-11}$ $\frac{5.8}{8}$ $\frac{5.0}{3}$ $\frac{5.1}{5}$ $\frac{5.7}{7}$ $\frac{6.6}{10-11}$ $\frac{4.8}{13}$ $\frac{3.5}{2.5}$

Staple in N.W. root 2nd Maple S. of DW. 81.51+3.0

+0.1 -0.1 -1.0 -0.4 0.0 0.0 -0.4 +1.1 +1.6
 $\frac{1.6}{25}$ $\frac{1.3}{13}$ $\frac{2.7}{10-9}$ $\frac{2.1}{7}$ $\frac{1.7}{7}$ $\frac{2.1}{11}$ $\frac{0.6}{17}$ $\frac{0.1}{2.5}$

+0.6 +0.3 -1.0 -0.4 0.0 -0.3 -1.1 +0.3 +0.7
 $\frac{0.1}{25}$ $\frac{0.4}{12}$ $\frac{1.7}{9}$ $\frac{1.1}{5}$ $\frac{0.7}{5}$ $\frac{1.0}{8}$ $\frac{1.3}{13}$ $\frac{0.4}{16}$ $\frac{0.0}{2.5}$

1208 61

53 - 1.7 06.9

54 - 4.5 04.1

55 7 - 7.3 01.3
T.F. 4.58 1205 68 7.51 1201.10

56 - 5.6 00.1

57 - 5.4 00.3

58 - 4.3 01.4

59 - 2.7 03.0

T.F. 9.47 1213 02 2.33 1203.35

B.M. 6.20 1206.82
60 - 7.8 05.2

61 - 4.0 09.0

17

$$\begin{array}{cccccccc} +1.2 & -0.4 & -0.5 & 0.0 & +0.3 & -0.3 & -1.3 & +0.6 \\ \hline 0.5 & 2.1 & 2.2 & 1.7 & 1.4 & 2.0 & 3.0 & 1.1 \\ 2.5 & 1.1 & 7 & & 4 & 10 & 14 & 17-2.5 \end{array}$$

$$\begin{array}{cccccccccccc} +1.5 & +0.4 & -1.3 & -0.3 & 0.0 & +0.4 & -0.2 & -1.3 & +0.1 & +0.5 \\ \hline 3.0 & 4.1 & 5.8 & 4.8 & 4.5 & 4.1 & 4.7 & 5.8 & 4.4 & 4.0 \\ 2.5 & 1.0 & 7 & 3 & 5 & 12 & 16 & 18 & 25 \end{array}$$

$$\begin{array}{cccccccccccc} +1.9 & +0.3 & -0.6 & 0.0 & +0.3 & -0.1 & -0.7 & +0.1 & +0.5 \\ \hline 5.7 & 7.0 & 7.9 & 7.3 & 7.0 & 7.4 & 8.0 & 7.2 & 6.8 \\ 2.5 & 9 & 6-5 & 6 & 12 & 12 & 14 & 25 \end{array}$$

$$\begin{array}{cccccccccccc} -0.7 & -0.2 & -0.4 & 0.0 & +0.3 & -0.2 & -1.1 & -0.7 & -1.4 \\ \hline 6.3 & 5.8 & 6.0 & 5.6 & 5.3 & 5.8 & 6.7 & 6.3 & 7.0 \\ 2.5 & 2 & 4 & & 7 & 13 & 18 & 19 & 25 \end{array}$$

$$\begin{array}{cccccccccccccccc} -2.9 & -2.0 & -1.9 & -1.1 & -0.7 & -0.2 & -0.5 & 0.0 & 0.0 & -0.3 & -1.1 & -1.4 & -0.8 & -1.2 \\ \hline 8.2 & 7.4 & 7.3 & 6.5 & 6.1 & 5.6 & 5.7 & 5.4 & 5.4 & 5.7 & 6.5 & 6.8 & 6.2 & 6.6 \\ 200 & 150 & 80 & 2.5 & 11 & 7 & 6 & 6 & 12 & 15-14 & 17 & 17 & 17 & 17 \\ & & & & & & & & & & & & & & 3.5 \\ & & & & & & & & & & & & & & 100 \end{array}$$

Road is water stred along here

Ditches should be opened into fields Rt. & Lt.

$$\begin{array}{cccccccccccc} -0.6 & -0.3 & -0.7 & 0.0 & +0.3 & -0.3 & -1.1 & -0.5 & -0.7 \\ \hline 4.9 & 4.6 & 5.0 & 4.3 & 4.0 & 4.0 & 5.4 & 4.8 & 5.0 \\ 2.5 & 2 & 5.4 & & 4 & 11 & 14-15 & 12 & 2.5 \end{array}$$

$$\begin{array}{cccccccccccc} +0.7 & +0.3 & -0.6 & -1.2 & 0.0 & +0.1 & -0.4 & -1.2 & -0.5 & +0.5 \\ \hline 2.0 & 2.4 & 3.3 & 3.4 & 2.1 & 2.6 & 3.1 & 3.9 & 3.2 & 2.1 \\ 2.5 & 14 & 11-7 & 6-5 & 2 & 3 & 9 & 13-14 & 15 & 2.5 \end{array}$$

04

Staple in W root 24" Maple 30'Rt. Sta 59+20

$$\begin{array}{cccccccccccccccc} 5.2 & 5.3 & 7.6 & 9.9 & 8.1 & 7.8 & 7.6 & 8.0 & 9.4 & 8.1 & 6.6 & 6.1 \\ \hline 2.5 & 12 & 12-7 & 8 & 4 & 0.0 & 3 & 8 & 13-14 & 15 & 2.1 & 2.5 \\ +2.6 & +2.5 & +0.2 & -1.6 & -0.3 & 0.0 & +0.2 & -0.2 & -1.6 & -0.3 & +1.1 & +1.7 \end{array}$$

$$\begin{array}{cccccccccccc} +2.3 & +2.1 & +0.2 & -2.2 & -0.6 & 0.0 & -0.3 & -1.4 & 0.0 & +1.1 \\ \hline 1.7 & 1.9 & 3.8 & 6.2 & 1.6 & 1.0 & 4.3 & 5.4 & 4.0 & 2.9 \\ 2.5 & 16 & 15-12 & 10-9 & 4 & 10 & 10 & 14-15 & 16 & 2.5 \end{array}$$

1217 70

70 - 4.9 12.9

T.F. 5.52 1217 73 5.55 1212.21

71 - 6.2 11.5

72 - 6.8 10.9

+11 12" C.M.P. Sec. 6.7 11.0

73 - 6.6 11.1

74 - 4.8 12.9

+30 - 4.3 13.4

75 - 6.1 11.6

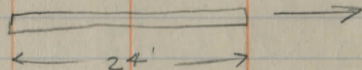
B.M. 33.9 1214.34

+0.2	-0.5	-1.5	-0.5	0.0	-0.3	-1.1	-0.3	-0.2
4.7	5.4	6.4	5.4	4.7	5.2	6.0	5.2	5.1
25	14	12	8	7	7	11	13	25

+1.2	-0.1	-1.2	-0.4	0.0	-0.3	-1.1	+0.3	+1.9
5.0	6.3	7.4	6.6	6.2	6.5	7.3	5.9	4.3
25	14	11	7	7	8	11	18	25

-1.0	-0.8	-1.8	-0.6	-0.1	0.0	-0.3	-1.4	-1.1	-1.8
7.8	7.6	8.6	7.4	6.9	6.8	7.1	8.7	7.9	8.6
25	17	16	14	9	6	8	12	14	25

-1.0	-0.9	-2.1	-1.8	-0.8	-0.1	0.0	-0.1	-1.6	-2.5	-2.5
2.7	7.6	8.3	8.5	7.5	6.8	6.7	8.9	8.3	9.2	9.2
25	18	17	13	12	10	9	9	11	11	25
			FL					FL		25' ditch

Good
cond

+0.4	-0.2	-1.0	-0.3	0.0	-0.6	-1.3	-0.2	-0.5
6.2	6.8	7.6	6.9	6.6	7.3	7.9	6.8	7.1
25	15	12	7	6	11	12	25	25

+1.2	-0.2	-1.2	-0.3	0.0	-0.6	-1.3	-0.1	+0.4	+1.1
3.6	5.0	6.0	5.1	4.8	5.4	6.1	4.9	4.4	3.7
25	14	10	7	7	9	13	14	17	25

+1.5	+0.4	-0.9	-0.2	0.0	+0.2	-0.1	-0.7	+0.2	+0.9
2.8	3.9	5.2	4.5	4.3	4.1	4.4	5.0	4.1	3.4
25	15	11	5	2	4	9	14	16	25

+3.7	+1.0	+0.1	-0.3	0.0	0.0	+0.1	-0.1	-1.2	+0.4	+0.9
2.4	5.1	6.0	6.4	6.1	6.1	6.0	6.2	7.3	5.7	5.2
25	12	10	8	5	5	5	11	15-16	17	25

Staple in N.W. root 18" Maple 30' Rt. Sta 74+60

1217 73

76 - 8.8 08.9

+40 - 9.5 08.2

77 - 10.7 07.0
T.F. 4.85 1211 34 1124 1206.49

78 - 5.0 06.3

+15 & 3' x 2 1/2' Con. Box 4.7 06.6

Temp. B.M. x N.W. Cor. W. Head Wall, 3.33 1208.01

79 - 4.2 07.1

80 - 2.0 09.3

+30 - 0.5 10.8

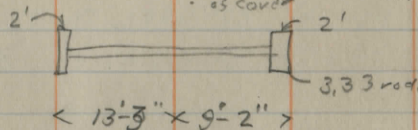
+3.7 +2.8 -0.2 +0.3 0.0 -0.1 -0.4 -1.2 -0.7 -0.4
 $\frac{5.1}{25} \frac{6.0}{15} \frac{9.0}{10} \frac{8.5}{7} \frac{8.8}{7} \frac{8.9}{7} \frac{9.2}{11} \frac{10.0}{15-16} \frac{9.5}{17} \frac{9.2}{25}$

+4.2 +3.4 -1.3 -0.5 0.0 +0.2 -0.5 -1.3 -0.7 -0.7
 $\frac{5.3}{25} \frac{6.1}{17} \frac{10.3}{8} \frac{10.0}{5} \frac{9.5}{4} \frac{9.3}{11} \frac{10.0}{15} \frac{10.8}{16} \frac{10.4}{12} \frac{10.2}{20-25}$

+1.6 +6.1 -1.0 -1.5 -0.5 0.0 0.0 -0.3 -1.3 -0.8
 $\frac{9.1}{25} \frac{9.6}{21} \frac{11.7}{14-15} \frac{12.1}{10-9} \frac{11.2}{5} \frac{10.7}{4} \frac{10.7}{10} \frac{11.0}{10} \frac{12.0}{15} \frac{11.5}{16-25}$

-1.2 -2.0 -1.0 -0.4 0.0 -0.2 -1.9 -1.1 -1.2
 $\frac{6.2}{25} \frac{7.0}{18} \frac{6.0}{16} \frac{5.4}{15-9} \frac{5.0}{7} \frac{5.2}{12} \frac{6.7}{12} \frac{6.1}{13} \frac{6.2}{18-25}$

0.0 -2.0 -3.3 -4.1
 $\frac{4.7}{7} \frac{6.7}{8} \frac{8.0}{8}$
 Bottom as cover 10 RL Dist Inlet to Drain Tile



-1.4 -1.0 -1.7 -1.4 -1.9 -0.7 0.0 0.0 -0.3 -0.6 -1.3 -1.0 -1.5
 $\frac{5.5}{25} \frac{5.9}{20} \frac{5.9}{18} \frac{5.6}{16} \frac{6.1}{15} \frac{4.9}{13} \frac{4.2}{4} \frac{4.5}{4} \frac{4.8}{7} \frac{5.5}{9} \frac{5.3}{10} \frac{5.7}{25}$

-0.8 +0.1 -0.1 +0.2 0.0 -0.3 -1.4 -1.8 -1.3
 $\frac{2.8}{25} \frac{1.7}{19} \frac{2.1}{15} \frac{1.8}{5} \frac{2.0}{4} \frac{2.3}{4} \frac{3.4}{8-12} \frac{3.8}{13-14} \frac{3.3}{16-25}$

0.0 +0.4 0.0 +0.4 -2.9
 $\frac{0.5}{17} \frac{0.1}{10} \frac{0.5}{5} \frac{0.1}{7} \frac{3.4}{13-14}$

J.F. 881 1221 10 1212.29
 80+45² 9.30 11.80
 + 52² 9.15 11.95
~~87~~ 59² 9.30 11.80
 81 - 9.0 11.5

x on. S.W. Cor S. Head Wall at X Rds.

S. edge Pavement
 E Pavement
 N. edge Pavement
 $\frac{103}{25} \frac{148}{23} \frac{107}{22} \frac{97}{11} \frac{95}{2} \frac{90}{2} \frac{103}{10} \frac{115}{14-16} \frac{83}{22} \frac{80}{25} -26$
 -0.7 -2.2 -1.1 -0.1 +0.1 0.0 -0.7 -1.9 ^{+1.3 +1.6}
 walk

+2.7 +1.5 +1.1 -1.7 -0.2 0.0 -0.1 -1.5 +1.3 +2.3
 $\frac{57}{25} \frac{69}{22} \frac{73}{18} \frac{101}{16-15} \frac{86}{9-4} \frac{84}{2} \frac{85}{8} \frac{92}{11-13} \frac{71}{16} \frac{61}{23} -26$
 walk

82 - 8.4 12.7

83 - 5.0 16.1

+1.7 +1.1 -1.3 -0.4 0.0 0.0 -1.5 -1.9 +0.2 +0.8
 $\frac{33}{25} \frac{39}{12} \frac{63}{12-10} \frac{54}{8} \frac{50}{2} \frac{50}{4} \frac{65}{8} \frac{69}{12-14} \frac{48}{16} \frac{42}{23} \text{walk}$

84 - 3.1 18.0

-0.7 -0.2 -0.8 -1.7 -0.7 -0.3 0.0 -0.5 -1.4 -0.4 +0.5
 $\frac{38}{25} \frac{38}{17} \frac{39}{13} \frac{48}{12-11} \frac{38}{7} \frac{37}{3} \frac{31}{3} \frac{36}{9} \frac{45}{12-14} \frac{35}{15} \frac{26}{24} \text{walk}$

85 - 1.4 19.7

+1.1 +0.2 -1.2 -0.5 0.0 0.0 -0.3 -0.5 -1.4 -0.2 +0.5 +1.3
 $\frac{03}{25} \frac{12}{12} \frac{26}{11-9} \frac{19}{2} \frac{14}{2} \frac{14}{3} \frac{17}{5} \frac{19}{9} \frac{28}{12-14} \frac{16}{15} \frac{09}{20} \frac{01}{24}$

J.F. 11.32 1232 19 0.23 1220.87
 86 - 9.0 23.2

+1.0 +0.3 -2.5 -0.5 0.0 -0.1 -1.5 0.0 +1.2
 $\frac{80}{25} \frac{87}{14} \frac{112}{13-12} \frac{95}{7} \frac{90}{2} \frac{91}{9} \frac{105}{14-15} \frac{90}{16-18} \frac{78}{27-30}$

87 - 5.9 26.3

+0.5 -0.3 -2.0 -0.4 0.0 +0.2 -0.1 -1.9 -0.4 +1.3
 $\frac{54}{25} \frac{62}{14} \frac{79}{12-11} \frac{63}{7} \frac{53}{2} \frac{57}{3} \frac{60}{10} \frac{73}{13-14} \frac{63}{16} \frac{46}{27-30}$

1232 19

88			- 4.1	28.1
B.M.			1.72	1230.47 ^{30.49}
89			- 2.5	29.7
T.P.	8.83	1239	94	1.08 1231.11
90			- 8.9	31.0
91			- 7.8	32.1
92			- 5.8	34.1
93			- 3.8	36.1
T.P.				
94			- 1.7	38.2
T.P.	11.97	1251	06	9.85 1239.09
95			- 10.5	40.6

20

+0.3 -0.1 -1.2 -0.4 0.0 +0.2 -0.2 -1.8 -0.8 +1.6
 $\frac{3.8}{25} \frac{4.2}{12} \frac{5.3}{11-10} \frac{4.5}{5} \frac{4.1}{4} \frac{3.9}{4} \frac{4.3}{9} \frac{5.9}{14-15} \frac{4.9}{16-19} \frac{3.5}{27-30}$

Staple in E. root 15" Maple 25' Lt. 88+90

+1.3 +0.3 -0.5 -1.8 -0.4 0.0 +0.2 -0.5 -2.1 -0.8 +1.5
 $\frac{1.2}{25} \frac{2.2}{16} \frac{3.0}{14-12} \frac{4.3}{11-10} \frac{2.9}{6} \frac{2.5}{6} \frac{2.3}{4} \frac{3.0}{10} \frac{4.6}{14-15} \frac{3.3}{12-19} \frac{1.0}{27}$

-0.3 -0.2 -1.7 -0.3 0.0 0.0 -0.2 -1.0 -0.2 +1.3
 $\frac{9.2}{25} \frac{8.1}{12} \frac{10.5}{11-10} \frac{9.2}{9} \frac{8.9}{9} \frac{8.7}{4} \frac{9.1}{10} \frac{9.9}{13-14} \frac{9.1}{15-18} \frac{7.5}{25}$

+0.6 +0.2 -0.9 -0.3 0.0 -0.2 -0.2 -0.9 0.0 +0.5 +1.7
 $\frac{7.2}{25} \frac{7.6}{12} \frac{8.7}{10-9} \frac{8.1}{7} \frac{7.8}{7} \frac{7.6}{3} \frac{8.0}{9} \frac{8.7}{12-13} \frac{7.8}{14} \frac{7.3}{21} \frac{6.1}{25}$

+0.3 -0.7 -1.4 -0.6 0.0 +0.2 -0.2 -1.1 -0.1 +0.2 +1.6
 $\frac{5.5}{25} \frac{6.5}{13} \frac{7.2}{12-10} \frac{6.4}{8} \frac{5.8}{8} \frac{5.6}{3} \frac{6.0}{10} \frac{6.9}{13-14} \frac{5.9}{15} \frac{4.0}{22} \frac{4.2}{25}$

-0.6 -1.1 -2.1 -0.7 0.0 0.0 -0.5 -1.3 -0.5 +0.8 +1.6
 $\frac{4.4}{25-20} \frac{4.9}{12} \frac{5.7}{11-10} \frac{4.5}{6} \frac{3.8}{4} \frac{3.8}{9} \frac{4.5}{13-14} \frac{5.1}{15} \frac{4.3}{20} \frac{3.0}{25} \frac{2.7}{25}$

-0.5 -0.8 -2.6 -0.6 0.0 +0.3 -0.2 -1.4 -0.2 0.0 +1.5
 $\frac{2.3}{25} \frac{2.5}{12} \frac{4.3}{11-10} \frac{2.3}{8} \frac{1.7}{8} \frac{1.4}{1-5} \frac{1.9}{10} \frac{3.1}{13-14} \frac{1.9}{15} \frac{1.7}{20} \frac{0.2}{25}$

+2.0 -0.3 -1.1 -0.5 0.0 +0.1 -0.2 -1.1 -0.1 +0.5 +1.3
 $\frac{8.5}{25} \frac{10.3}{12} \frac{11.6}{11-9} \frac{11.0}{7} \frac{10.5}{7} \frac{10.4}{2-5} \frac{10.7}{10} \frac{11.6}{13-14} \frac{10.6}{15} \frac{10.0}{21} \frac{9.2}{25}$

12.51.06

96 - 7.8 43.3

97 - 4.4 46.7

T.F. 11.29 1262.34 0.71 1250.35
98 - 9.4 52.9

99 - 2.1 60.2

10-12-21
windy-cloudy-cold-rain

T.F. 11.63 1272 73 1.24 1261.10
+25 - 10.5 62.2

170 - 8.7 64.0

100 - 6.8 65.9

+75 - 4.1 68.6

101 - 4.8 67.9

+1.2 +0.2 -1.1 -0.3 0.0 +0.1 -0.3 -0.7 +0.1 +0.6 +2.3
 $\frac{6.6}{25} \frac{7.6}{11} \frac{8.9}{10-9} \frac{8.1}{7} \frac{7.8}{4} \frac{7.7}{11} \frac{8.1}{14-15} \frac{8.5}{17} \frac{7.7}{21} \frac{7.2}{26} \frac{5.5}{26}$

+3.4 +1.5 -1.3 -0.4 0.0 +0.2 -0.4 -1.1 +0.6 +4.1
 $\frac{1.0}{25-20} \frac{2.9}{11} \frac{5.7}{9-8} \frac{4.8}{5} \frac{4.4}{6} \frac{4.2}{11} \frac{4.8}{14-15} \frac{5.5}{16} \frac{3.8}{26} \frac{0.3}{26}$

+4.4 +4.1 +2.4 +2.2 -1.0 -0.1 0.0 +0.3 0.0 -1.2 +2.8 +2.9
 $\frac{5.0}{25} \frac{5.3}{21} \frac{7.0}{16} \frac{7.2}{13} \frac{10.8}{10-9} \frac{9.5}{8} \frac{9.4}{8-6} \frac{9.1}{11} \frac{9.4}{15-16} \frac{10.6}{22} \frac{6.6}{26} \frac{6.5}{26}$

+3.1 +2.6 +2.1 +1.2 -0.1 0.0 +0.1 +0.5 -0.3 +0.6 +0.8
 $\frac{1.0}{25} \frac{0.5}{22} \frac{0.0}{14} \frac{0.9}{10} \frac{2.2}{9} \frac{2.1}{5} \frac{2.0}{13} \frac{1.6}{16} \frac{2.4}{17} \frac{1.5}{19} \frac{1.3}{26}$

+1.0 +0.2 0.0 +0.2 0.0 -1.5 0.0 -0.1
 $\frac{9.5}{25} \frac{10.3}{17} \frac{10.5}{3} \frac{10.3}{15} \frac{10.5}{17} \frac{12.0}{19} \frac{10.5}{26} \frac{10.6}{26}$

+3.3 +2.9 +2.0 +1.6 -0.9 -0.3 0.0 -0.1 -0.7 -0.2 +0.4
 $\frac{5.4}{25} \frac{5.8}{19} \frac{6.7}{17} \frac{7.1}{15} \frac{9.6}{12} \frac{9.0}{10} \frac{8.1}{10} \frac{8.8}{10} \frac{9.4}{13-14} \frac{8.7}{16} \frac{8.3}{26}$

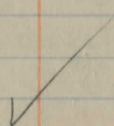
+2.1 +1.2 -1.3 -0.2 0.0 -0.5 -1.4 -1.0 -0.1
 $\frac{4.7}{25} \frac{5.6}{16} \frac{8.1}{14} \frac{7.0}{7} \frac{6.8}{10} \frac{7.3}{14} \frac{8.2}{15} \frac{7.8}{26} \frac{6.7}{26}$

-0.5 -0.8 -1.4 -0.6 0.0 -0.7 -1.7 -1.0 -0.8
 $\frac{4.6}{25} \frac{4.9}{15} \frac{5.5}{14-13} \frac{4.7}{8} \frac{4.1}{8} \frac{4.8}{12+13} \frac{5.3}{14} \frac{5.1}{14} \frac{4.9}{27}$

-0.2 -0.8 -1.6 -0.6 0.0 -0.5 -1.7 -1.3 0.0 +0.2
 $\frac{5.0}{25} \frac{5.6}{16} \frac{6.4}{14} \frac{5.4}{14} \frac{4.8}{14} \frac{5.3}{7} \frac{6.5}{12-13} \frac{6.1}{14-15} \frac{4.8}{17-19} \frac{4.4}{27}$

1272 73

102			-	9.0	63.1
B. M.				6.42	1266.31
T. P.	1.14	1262	50	11.37	1261.36
103			-	3.0	58.9
104			-	8.5	54.0
105			✓	11.8	50.7
T. P.	1.76	1251	72	12.57	1249.96
106			-	2.5	49.2
107			-	4.8	46.9
108			-	8.6	43.1
T. P.	1.43	1241	86	11.29	1240.43
109				1.1	40.5



+0.5	-0.6	-1.7	-0.6	0.0	-0.5	-1.6	+0.2	+0.9	+2.2
$\frac{91}{25}$	$\frac{107}{16}$	$\frac{113}{15-14}$	$\frac{102}{10}$	$\frac{96}{-}$	$\frac{101}{7}$	$\frac{113}{10-11}$	$\frac{94}{15}$	$\frac{87}{22}$	$\frac{74}{27}$

Staple in W. root 24" Elm, 35" Rt., 102+18

+1.2	+0.8	-0.2	-0.5	-0.2	0.0	-0.5	-1.3	-0.4	+1.4	+1.5
$\frac{2428}{25}$	$\frac{38}{18}$	$\frac{38}{16}$	$\frac{71}{15}$	$\frac{38}{7-3}$	$\frac{30}{-}$	$\frac{41}{6}$	$\frac{49}{9-10}$	$\frac{40}{12}$	$\frac{27}{25}$	$\frac{21}{27}$

+1.1	+0.6	-0.2	-1.2	-0.4	0.0	0.0	-0.4	-2.0	-0.3	+0.1	+1.0
$\frac{74}{25}$	$\frac{79}{19}$	$\frac{87}{16}$	$\frac{27}{15-14}$	$\frac{89}{11}$	$\frac{85}{2}$	$\frac{85}{-}$	$\frac{87}{6}$	$\frac{105}{10-11}$	$\frac{88}{12}$	$\frac{84}{20}$	$\frac{75}{27}$

+0.2	-0.1	-0.6	0.0	0.0	-0.2	-1.2	-0.4	-1.5	+0.4
$\frac{116}{25}$	$\frac{119}{18}$	$\frac{124}{16-15}$	$\frac{118}{12}$	$\frac{118}{-}$	$\frac{120}{6}$	$\frac{130}{10-11}$	$\frac{122}{12}$	$\frac{133}{17-16}$	$\frac{117}{27}$

+0.6	-0.3	-1.3	-0.4	0.0	-0.6	-1.5	-1.0	-1.1	-0.4
$\frac{19}{25}$	$\frac{23}{18}$	$\frac{44}{17-16}$	$\frac{29}{14}$	$\frac{25}{-}$	$\frac{31}{6}$	$\frac{40}{9-10}$	$\frac{35}{11}$	$\frac{40}{18-17}$	$\frac{29}{27}$

+0.2	-0.5	-1.7	-0.4	0.0	-0.6	-2.0	-0.3	+0.2
$\frac{44}{25}$	$\frac{53}{18}$	$\frac{65}{17-16}$	$\frac{52}{12}$	$\frac{18}{-}$	$\frac{54}{7}$	$\frac{68}{11-12}$	$\frac{51}{16}$	$\frac{46}{27}$

+0.1	-0.4	-1.7	-0.6	0.0	-0.5	-1.7	+0.1	+0.6	+1.7
$\frac{35}{25}$	$\frac{90}{17}$	$\frac{103}{16-15}$	$\frac{92}{11}$	$\frac{86}{-}$	$\frac{91}{7}$	$\frac{103}{12-13}$	$\frac{85}{16}$	$\frac{80}{21}$	$\frac{69}{27}$

+0.3	-0.8	-1.3	-0.6	0.0	-0.2	-1.5	0.0	+0.8	+1.6
$\frac{11}{25}$	$\frac{27}{16}$	$\frac{27}{15-14}$	$\frac{20}{12}$	$\frac{14}{-}$	$\frac{16}{7}$	$\frac{29}{11-12}$	$\frac{14}{14}$	$\frac{06}{20}$	$\frac{-02}{27}$

1241 86

110 - 3.6 38.3

111 - 5.6 36.3

B.M. 5.12 1236.74

112 - 6.6 35.3

113 - 8.6 33.3

T.F. 0.81 1233.20 9.47/23.239
114 - 3.3 29.9

115 5.8 27.6

+69 ± 2'x2' stone Box 5.8 27.4

Rev (Use old stone for new)
Headwalls 2x2 Box Can

25

$$\begin{array}{cccccccccccc} -0.4 & -1.6 & -0.5 & 0.0 & +0.2 & -0.5 & -1.5 & -0.3 & +1.2 \\ 25 & \frac{40}{14} & \frac{5.2}{12} & \frac{4.1}{9} & \frac{3.6}{2} & \frac{3.4}{9} & \frac{4.1}{9} & \frac{5.1}{13-15} & \frac{3.9}{18} & \frac{2.4}{20} \end{array}$$

$$\begin{array}{cccccccccccc} -0.7 & -0.6 & -1.3 & -0.4 & 0.0 & +0.2 & -0.3 & -1.1 & -0.1 & +0.9 \\ 25 & \frac{6.3}{14} & \frac{6.2}{13} & \frac{6.9}{12} & \frac{6.0}{9} & \frac{5.6}{3} & \frac{5.4}{10} & \frac{5.9}{13-15} & \frac{6.7}{17} & \frac{5.7}{23} & \frac{4.7}{27} \end{array}$$

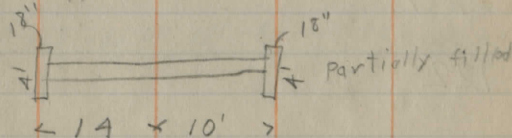
Staple in w. root 10" Maple, 23' RT 111+20

$$\begin{array}{cccccccccccc} -0.2 & -0.8 & -1.7 & -0.5 & 0.0 & -0.4 & -1.8 & -0.5 & +0.2 \\ 25 & \frac{6.8}{14} & \frac{7.4}{12-11} & \frac{8.5}{8} & \frac{7.1}{8} & \frac{6.6}{9} & \frac{7.0}{12-13} & \frac{8.4}{14} & \frac{7.1}{14} & \frac{6.4}{27} \end{array}$$

$$\begin{array}{cccccccccccc} +0.2 & -0.1 & -1.4 & -2.0 & -0.8 & 0.0 & -0.5 & -1.6 & -0.5 & +0.4 \\ 25 & \frac{8.4}{17} & \frac{8.7}{14} & \frac{10.0}{13-12} & \frac{10.6}{8} & \frac{9.4}{8} & \frac{8.6}{8} & \frac{9.1}{12-13} & \frac{10.2}{15} & \frac{9.1}{27} \end{array}$$

$$\begin{array}{cccccccccccc} +1.2 & -0.1 & -1.2 & -2.0 & -0.8 & 0.0 & -0.9 & -2.2 & -1.1 & -0.4 & +0.2 & +1.4 \\ 25 & \frac{2.1}{22} & \frac{3.4}{14} & \frac{4.5}{13-12} & \frac{5.3}{8} & \frac{4.1}{8} & \frac{3.3}{8} & \frac{4.2}{8} & \frac{5.5}{12-13} & \frac{4.4}{14} & \frac{3.7}{13} & \frac{3.1}{20} & \frac{1.9}{27} \end{array}$$

$$\begin{array}{cccccccccccc} -1.0 & -0.5 & -1.3 & -0.1 & 0.0 & -0.4 & -1.7 & -0.6 & -0.4 & +0.9 \\ 25 & \frac{6.6}{16} & \frac{6.1}{14-13} & \frac{6.9}{9} & \frac{5.7}{9} & \frac{5.6}{9} & \frac{6.0}{8} & \frac{7.3}{12-17} & \frac{6.7}{20} & \frac{6.0}{23} & \frac{4.7}{27} \end{array}$$

$$\begin{array}{cccccccccccc} -4.7 & -3.8 & -3.1 & -0.5 & 0.0 & -0.5 & -2.7 & -2.6 \\ 75 & \frac{10.5}{25} & \frac{9.6}{25} & \frac{8.9}{15} & \frac{6.3}{13} & \frac{5.8}{13} & \frac{6.3}{8} & \frac{8.5}{10} & \frac{8.1}{10} & \frac{8.1}{20} \end{array}$$
No floor
Foot Cont

1233 20

116 - 6.6 26.6

117 - 5.6 27.6

T.P. 1.57 1229 14 5.63 1227.57
+50 - 2.2 26.9

118 - 4.1 25.0

119 - 7.9 21.2

120 - 11.9 17.2

T.P. 2.10 1218 22 13.02 1216.12
121 - 3.7 14.5

B.M. 7.30 1210.92

122 - 5.4 12.8

✓

✓

$$-2.1 \quad -0.9 \quad -1.0 \quad -0.4 \quad 0.0 \quad -0.4 \quad -1.6 \quad -1.1 \quad -0.7 \quad 0.0 + 1.2$$

$$\frac{8.7}{25} \quad \frac{7.5}{14} \quad \frac{7.6}{13} \quad \frac{7.0}{12} \quad \frac{6.6}{8} \quad \frac{7.0}{10} \quad \frac{8.3}{12} \quad \frac{7.7}{13} \quad \frac{7.3}{19} \quad \frac{6.6}{20} \quad \frac{5.4}{22}$$

$$-0.4 \quad -1.3 \quad -0.6 \quad 0.0 \quad -0.3 \quad -0.8 \quad +0.1 \quad +0.3$$

$$\frac{6.0}{25} \quad \frac{6.9}{14} \quad \frac{6.2}{11} \quad \frac{5.6}{8} \quad \frac{5.9}{7} \quad \frac{6.4}{15} \quad \frac{5.5}{12} \quad \frac{5.3}{27}$$

$$+0.5 \quad -0.2 \quad -0.9 \quad -0.3 \quad 0.0 \quad +0.2 \quad -0.3 \quad -1.2 \quad -0.6 \quad +0.1$$

$$\frac{1.7}{25} \quad \frac{2.4}{10} \quad \frac{3.1}{7.8} \quad \frac{2.5}{7} \quad \frac{2.2}{2.1} \quad \frac{2.0}{4} \quad \frac{2.5}{11} \quad \frac{3.4}{15} \quad \frac{2.8}{16} \quad \frac{2.1}{27}$$

$$+2.5 \quad +1.7 \quad -0.2 \quad 0.0 \quad +0.3 \quad -0.1 \quad -0.6 \quad -0.1 \quad +0.7$$

$$\frac{1.6}{25} \quad \frac{2.4}{14} \quad \frac{1.3}{9} \quad \frac{4.1}{1} \quad \frac{3.8}{5} \quad \frac{4.2}{13} \quad \frac{4.7}{16} \quad \frac{4.2}{18} \quad \frac{3.4}{27}$$

$$+2.5 \quad +1.9 \quad +0.1 \quad -1.5 \quad -0.3 \quad 0.0 \quad +0.4 \quad -0.3 \quad -1.2 \quad -0.7 \quad +0.9$$

$$\frac{5.4}{25} \quad \frac{6.0}{17} \quad \frac{7.8}{11} \quad \frac{9.4}{10.9} \quad \frac{8.2}{7} \quad \frac{7.9}{5} \quad \frac{2.5}{11} \quad \frac{8.2}{11} \quad \frac{9.1}{14} \quad \frac{8.6}{15} \quad \frac{7.0}{12} \quad \frac{7.0}{27}$$

$$+1.4 \quad +0.6 \quad -0.5 \quad -1.1 \quad -0.4 \quad 0.0 \quad +0.2 \quad -0.2 \quad -1.2 \quad -0.6 \quad -0.1 \quad +1.0$$

$$\frac{10.5}{25} \quad \frac{11.3}{12} \quad \frac{12.4}{12} \quad \frac{13.0}{11} \quad \frac{12.3}{10} \quad \frac{11.9}{7} \quad \frac{15.7}{4} \quad \frac{14.1}{10} \quad \frac{13.1}{13} \quad \frac{12.5}{14} \quad \frac{12.0}{15} \quad \frac{10.9}{21} \quad \frac{10.9}{25}$$

$$+1.1 \quad +0.2 \quad -1.6 \quad -0.3 \quad 0.0 \quad +0.2 \quad -0.3 \quad -1.4 \quad -0.4 \quad +0.7$$

$$\frac{2.6}{25} \quad \frac{3.5}{14} \quad \frac{5.3}{12} \quad \frac{4.0}{11} \quad \frac{4.0}{7} \quad \frac{3.7}{3} \quad \frac{3.5}{10} \quad \frac{4.0}{10} \quad \frac{5.1}{14} \quad \frac{4.1}{15} \quad \frac{3.0}{22} \quad \frac{3.0}{27}$$

$$+0.3 \quad -0.4 \quad -1.3 \quad -0.4 \quad 0.0 \quad +0.1 \quad -0.5 \quad -1.7 \quad -0.6 \quad -0.7 \quad 0.0$$

$$\frac{5.1}{25} \quad \frac{5.7}{14} \quad \frac{6.7}{12} \quad \frac{5.3}{11} \quad \frac{5.4}{7} \quad \frac{5.3}{3} \quad \frac{5.9}{10} \quad \frac{7.1}{14} \quad \frac{6.0}{14} \quad \frac{6.1}{15} \quad \frac{5.4}{22} \quad \frac{5.4}{25}$$

1218 22

123 - 6.2 12.0

windy

S.P. 0.92 1211 84 7.30 1210.92

124 - 2.2 09.6

+30 3.6 08.2

125 - 5.2 06.6

126 - 6.7 05.1

127 8.3 03.5

T.F. 2.77 1203.97 10.64 1201.20

128 - 2.1 01.9

129 - 4.0 00.0

27

-0.4	-0.5	-2.3	-0.3	00	-0.9	-2.7	-1.8	-0.9
$\frac{66}{75}$	$\frac{67}{16}$	$\frac{85}{14-13}$	$\frac{65}{10}$	$\frac{62}{11}$	$\frac{71}{11}$	$\frac{89}{15-16}$	$\frac{80}{17}$	$\frac{71}{27}$

Between 123 & 124 deduct 40', for culverts that lead to Rd RY Lt., from ditch Exc.

+0.6	00	-0.2	+0.4
$\frac{16}{25}$	$\frac{16}{12}$	$\frac{22}{10}$	$\frac{24}{21-25}$

+2.0	+1.3	-1.0	-0.1	00	-0.2	-2.0	+1.2
$\frac{16}{25}$	$\frac{23}{19}$	$\frac{46}{16-14}$	$\frac{37}{14}$	$\frac{36}{12}$	$\frac{32}{17-18}$	$\frac{56}{23-25}$	$\frac{24}{25}$

-0.7	-0.5	-1.8	-0.5	00	-0.6	-1.8	-0.8	+0.6
$\frac{59}{25}$	$\frac{57}{14}$	$\frac{70}{13}$	$\frac{57}{8}$	$\frac{52}{12}$	$\frac{58}{15-16}$	$\frac{70}{17}$	$\frac{60}{25}$	$\frac{85}{25}$

-0.9	-0.7	-1.8	-0.6	00	-0.5	-2.4	-1.1	-0.9
$\frac{76}{25}$	$\frac{74}{15}$	$\frac{85}{14-13}$	$\frac{73}{10}$	$\frac{67}{11}$	$\frac{72}{15-16}$	$\frac{91}{17}$	$\frac{78}{25}$	$\frac{76}{25}$
-0.1	-1.0	-2.0	-0.7	00	-0.4	-2.8	-1.7	-1.3
$\frac{84}{25}$	$\frac{93}{14}$	$\frac{103}{13-12}$	$\frac{90}{9}$	$\frac{83}{11}$	$\frac{87}{16-17}$	$\frac{118}{18}$	$\frac{100}{25}$	$\frac{96}{25}$

0.0	-0.7	-1.8	-0.6	00	-0.5	-2.1	-1.4	-1.0
$\frac{21}{25}$	$\frac{28}{15}$	$\frac{39}{14-13}$	$\frac{27}{9}$	$\frac{21}{13}$	$\frac{26}{15-16}$	$\frac{42}{17-18}$	$\frac{35}{16-17}$	$\frac{31}{25}$

+0.4	-1.0	-1.6	-0.3	0.0	+0.2	-0.4	-1.9	-1.2	-0.6
$\frac{36}{25}$	$\frac{50}{16-14}$	$\frac{56}{12-11}$	$\frac{43}{7}$	$\frac{40}{11}$	$\frac{38}{3}$	$\frac{44}{14}$	$\frac{59}{17-18}$	$\frac{52}{19}$	$\frac{46}{25}$

1203 9.7

130 - 5.4 98.6

131 - 6.2 97.8

B.M.
132 - 7.29 1196.68
- 7.3 96.7T.F.
133 2.69 1198.55 - 8.11 1195.86
- 2.8 95.8

134 - 3.7 95.2

+60 3.7 94.9

135 - 5.0 93.6

136 - 6.2 92.4

TR 2.19 1194.36 6.38 1192.17

✓

✓

$$\begin{array}{cccccccccccc} -0.7 & -0.6 & -1.4 & -0.6 & 0.0 & +0.3 & -0.4 & -1.6 & -0.8 & -0.3 \\ \frac{6.1}{25} & \frac{6.0}{14} & \frac{6.8}{13} & \frac{6.0}{12} & \frac{5.4}{8} & \frac{5.1}{3} & \frac{5.8}{13} & \frac{7.0}{16} & \frac{6.2}{18} & \frac{5.7}{25} \end{array}$$

$$\begin{array}{cccccccccccc} -0.7 & -0.8 & -1.8 & -0.7 & 0.0 & -0.4 & -1.6 & -1.0 & -0.7 & +0.2 \\ \frac{6.9}{25} & \frac{7.0}{15} & \frac{8.0}{14} & \frac{6.9}{13} & \frac{0.2}{10} & \frac{6.6}{12} & \frac{7.8}{15} & \frac{7.8}{16} & \frac{6.9}{17} & \frac{6.0}{21} & \frac{6.0}{25} \end{array}$$

Staple in W. root 30" Elm 30" Rt. 131180

$$\begin{array}{cccccccccccc} -1.1 & -0.8 & -2.0 & -0.9 & 0.0 & -0.4 & -1.5 & -0.2 & 0.0 \\ \frac{8.4}{25} & \frac{8.1}{16} & \frac{9.8}{14} & \frac{8.2}{13} & \frac{7.3}{10} & \frac{7.7}{12} & \frac{8.8}{15} & \frac{7.5}{16} & \frac{7.3}{25} \end{array}$$

$$\begin{array}{cccccccccccc} -1.0 & -2.0 & -0.6 & 0.0 & +0.2 & -0.4 & -1.8 & -0.8 & -0.5 \\ \frac{3.8}{25} & \frac{4.8}{15} & \frac{3.4}{13} & \frac{2.8}{8} & \frac{2.6}{4} & \frac{3.2}{12} & \frac{4.6}{16} & \frac{3.6}{17} & \frac{3.3}{25} \end{array}$$

$$\begin{array}{cccccccccccc} -1.3 & -1.4 & -2.2 & -1.1 & 0.0 & +0.3 & -0.7 & -2.3 & -1.1 & -0.6 \\ \frac{4.7}{25} & \frac{4.8}{14} & \frac{5.6}{13} & \frac{4.5}{8} & \frac{3.4}{3} & \frac{3.1}{7} & \frac{4.1}{14} & \frac{5.7}{17} & \frac{4.5}{19} & \frac{4.0}{25} \end{array}$$

$$\begin{array}{cccccccccccc} -1.3 & -1.6 & -2.8 & -1.0 & 0.0 & +0.2 & -0.7 & -2.2 & -1.3 \\ \frac{5.0}{25} & \frac{5.3}{14} & \frac{6.5}{13} & \frac{4.7}{8} & \frac{3.7}{3} & \frac{3.5}{7} & \frac{4.4}{14} & \frac{5.9}{17} & \frac{5.0}{20} & \frac{5.0}{25} \end{array}$$

$$\begin{array}{cccccccccccc} -0.1 & -0.5 & -1.7 & -2.2 & -0.6 & 0.0 & +0.3 & -0.2 & -1.9 & -0.7 & 0.0 \\ \frac{5.1}{25} & \frac{5.5}{15} & \frac{6.7}{13} & \frac{7.2}{11} & \frac{5.6}{8} & \frac{5.0}{5} & \frac{4.1}{3} & \frac{5.2}{14} & \frac{6.9}{17} & \frac{5.7}{20} & \frac{5.0}{25} \end{array}$$

$$\begin{array}{cccccccccccc} -1.2 & -1.0 & -1.8 & -0.3 & 0.0 & +0.4 & -0.4 & -1.4 & -0.7 & -0.2 \\ \frac{7.4}{25} & \frac{7.2}{13} & \frac{8.0}{11} & \frac{6.5}{9} & \frac{6.2}{4} & \frac{5.8}{4} & \frac{6.6}{14} & \frac{7.6}{16} & \frac{6.9}{18} & \frac{6.4}{25} \end{array}$$

1194.36

137 - 2.4 92.0

138 - 3.2 91.2

+50 4.2 90.2

139 - 4.9 89.5

140 - 6.0 88.4

141 - 6.3 88.1

T.F. 3.77 1191.45 6.68 1187.68

142 - 3.6 87.9

143 AB 86.7

+73
 1 1/2 x 2 stone
 Poor Cond.
 Remove ✓
 4.1 87.4 ✓

-1.6 -1.4 -2.0 -0.8 0.0 +0.3 -0.5 -1.3 -1.0 -0.7
 $\frac{4.0}{25}$ $\frac{3.8}{14}$ $\frac{4.4}{12}$ $\frac{3.2}{11}$ $\frac{2.4}{1}$ $\frac{2.1}{4}$ $\frac{2.9}{14}$ $\frac{3.7}{15}$ $\frac{3.4}{16}$ $\frac{3.1}{25}$

-0.7 -0.5 -2.2 -0.9 0.0 -1.0 -2.2 +0.8 +1.1
 $\frac{3.7}{25}$ $\frac{3.7}{15}$ $\frac{5.4}{12-11}$ $\frac{4.1}{10}$ $\frac{3.2}{1}$ $\frac{4.2}{13}$ $\frac{5.4}{16-17}$ $\frac{2.8}{21}$ $\frac{2.1}{25}$

+1.9 -1.1 -1.9 -0.8 0.0 +0.2 -0.4 -1.8 +1.5 +1.6
 $\frac{2.8}{25-18}$ $\frac{5.3}{15-13}$ $\frac{6.1}{12-11}$ $\frac{5.0}{9}$ 4.2 $\frac{4.0}{3}$ $\frac{4.6}{11}$ $\frac{6.0}{15-16}$ $\frac{3.7}{21}$ $\frac{2.6}{25}$

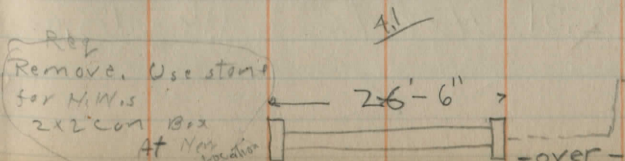
+1.4 +1.3 -0.7 -1.6 -0.7 0.0 +0.3 -0.9 -1.6 +0.4 +0.8
 $\frac{3.5}{25}$ $\frac{3.5}{18}$ $\frac{5.5}{15-13}$ $\frac{6.5}{12-11}$ $\frac{5.6}{8}$ $\frac{4.9}{1}$ $\frac{4.6}{5}$ $\frac{5.8}{12}$ $\frac{6.5}{13-15}$ $\frac{4.5}{20}$ $\frac{4.1}{25}$

-1.0 -0.7 -1.4 -0.6 0.0 -0.5 -1.4 -0.9 -0.6 -1.0
 $\frac{7.0}{25}$ $\frac{6.7}{17-15}$ $\frac{7.4}{13-12}$ $\frac{6.6}{10}$ $\frac{6.0}{1}$ $\frac{6.5}{11}$ $\frac{7.4}{14-15}$ $\frac{6.9}{16}$ $\frac{6.6}{20}$ $\frac{7.0}{25}$

-0.8 -1.1 -1.9 -0.7 0.0 -0.5 -2.0 -1.3
 $\frac{7.1}{25}$ $\frac{7.4}{16}$ $\frac{8.2}{15}$ $\frac{7.0}{13}$ $\frac{6.3}{1}$ $\frac{6.8}{9}$ $\frac{8.3}{13-14}$ $\frac{7.6}{15-25}$

-0.4 -0.3 -2.1 -1.2 0.0 -0.8 -2.1 -1.5 -1.0
 $\frac{4.0}{25}$ $\frac{3.9}{17}$ $\frac{5.7}{14-13}$ $\frac{4.8}{11}$ $\frac{3.6}{1}$ $\frac{4.4}{10}$ $\frac{5.7}{14-15}$ $\frac{5.1}{17}$ $\frac{4.6}{25}$

-0.2 -1.6 -0.7 0.0 -0.5 -1.7 -0.6 -0.7
 $\frac{5.0}{25-15}$ $\frac{6.4}{14-13}$ $\frac{5.5}{9}$ $\frac{4.7}{1}$ $\frac{5.7}{12}$ $\frac{6.5}{16-17}$ $\frac{5.4}{18}$ $\frac{5.5}{25}$



1191 ⁵45

144
+45 New Location for
2x2 con Box

5.3 86.2

144 - 5.0 86.5

B.M. 4.10 1187.35

145 - 5.1 86.4

146 - 7.3 84.2

T.P. 2.33 1185.01 8.77 1182.68

147 - 2.8 82.2

148 - 4.0 81.0

+50 5.4 79.6

149 - 7.9 77.1

T.P. 2.31 1178.16 9.6 1175.85



-0.3 -0.7 -0.2 0.0 +0.2 -0.3 -2.3 -3.3 -4.6
5.6 6.0 5.5 5.3 5.1 5.6 7.6 8.6 9.9
25 13 9 4 13 17 75 125

New Location

-0.6 -0.8 -1.0 -0.4 0.0 -0.2 -2.0 -0.6 -1.4
5.6 5.8 6.5 5.4 5.0 5.2 7.1 5.6 6.4
25 16 12-11 8 12 15-16 78-80 25

Staple in S. E. front 18" Locust 30" Lt. 144+60

+1.6 -0.0 -0.8 -1.0 -0.6 0.0 -0.4 -0.3 +0.3
3.5 5.1 5.9 6.1 5.7 5.1 5.5 5.4 4.8
25-23 19 10 9 6 12 20 21-25

+1.8 +0.4 -1.8 -0.5 0.0 +0.3 -0.3 -1.1 +0.1 -0.6
5.5 6.9 3.1 7.8 7.3 7.0 7.6 8.4 7.3 7.9
25 14 9-8 5 7 6 12 16-19 21-23 25

+0.1 -1.2 -1.5 -0.5 0.0 +0.3 -0.3 -1.4 -0.3 -1.2
2.7 4.0 4.3 3.3 2.8 2.5 3.1 4.2 3.1 4.0
25 4-11 10-9 5 5 5 11 15-16 18-22 25-23

+0.2 -0.7 -1.6 -0.6 0.0 0.0 -0.5 -1.3 -0.2 -0.7
3.8 4.7 5.6 4.6 4.0 4.0 4.5 5.3 4.2 4.7
25 12 11-10 7 5 11 13-14 17-21 22-25

+2.0 -1.0 -2.1 -0.4 0.0 -0.3 -1.9 -0.2 +0.3
3.4 6.4 7.5 5.8 5.4 5.7 7.3 5.6 5.1
25-22 15 14-13 9 18 13-14 75 25

+5.5 -1.3 -0.3 0.0 -0.4 -1.2 +2.4 +4.5 +5.2
2.4 4.2 8.1 7.9 8.3 9.1 5.5 3.4 2.7
30-28 15 14 11 8 10 16 25 26-30

This hill is
very stiff
Clay
1:1.5 slope easily

1178 16

150 - 88 69.4

+50 12.8 65.4

T.F. 1.01 1166 42 12.75 1165.41
151 - 6.2 60.2

T.F. 0.20 1157 38 9.24 1157.18
152 - 3.9 53.5

153 - 6.3 51.1

+58 3 1/2 x 4' Stone Box floor

(filled with about 1 ft of mud)

Temp B.M. 6.15 1158.48 5.05 1152.33

154 - 7.2 51.3



Lt. E Rt

+8.0	+8.5	-0.3	+0.3	0.0	-0.4	-1.5	+8.4	+8.8
0.8	0.3	0.1	0.5	0.8	0.7	10.3	0.4	0.0
3.0	2.5	1.6	1.2	4	7	20	25-30	

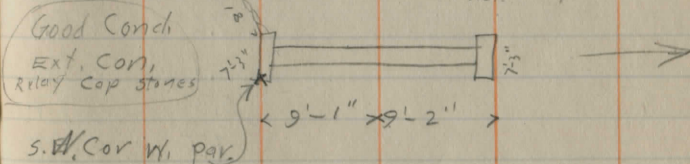
16.4	-1.2	0.0	0.0	-0.2	-0.9	+8.6	+8.8
6.4	14.0	12.8	12.8	13.0	13.7	9.2	4.0
30-25	13	15	12	2	8	21	30

+4.5	-0.7	0.0	0.0	-0.4	-1.3	+2.6	+4.6
1.7	6.9	6.2	6.2	6.6	7.5	3.6	1.6
2.8	19-18	12	6.2	6	10	15	2.5

-1.4	-0.6	-1.5	-0.4	0.0	0.0	-0.3	-0.9	-0.4	+0.6	+1.2
5.3	7.5	5.4	4.3	3.9	3.9	4.2	4.8	4.3	3.3	2.7
2.5	19	17-16	13	5	3.9	6	11	12-14	12	2.5

-1.9	-0.6	-0.7	-1.6	-0.2	0.0	-0.5	-1.8	-1.4	-2.7
8.2	7.9	7.2	7.7	6.5	6.3	6.8	8.1	7.7	9.0
2.5	19	18-16	15-14	9	6	11-12	13	2.5	

2.1
8.7
Bot. cover stone
Average of ground



-1.9	-0.9	-1.3	-0.5	0.0	0.0	-0.5	-1.1	-0.7	-1.7
9.1	8.1	8.5	7.7	7.2	7.2	7.7	8.3	7.9	8.9
2.5	11	10.9	6	6	6	9	11-12	13	2.5

5
1158 48

155 - 4.2 54.3

+25 2.8 55.7

T.P. 9.85 1166 64 1.69 1156.79
156 - 8.6 58.0

157 - 5.6 61.0

158 - 3.5 63.1

T.P. 7.79 1172 73 1.70 1164.94
+70 6.9 65.8
7.6 65.1
9.4 63.3
5.3 67.4
4.7 68.0

159 - 6.0 66.7

T.P. 8.79 1179.70 2.82 1169.91

-0.5 +0.2 -1.2 -2.4 -0.4 0.0 +0.2 -0.1 -1.3 +3.0
47 40 54 66 46 42 40 43 55 1.1
25 18 10 9 7 4 10 14-15 23-25

+4.5 +2.8 -2.4 -0.6 0.0 +0.3 -0.4 -1.5 +2.3
-17 0.0 5.2 3.4 2.8 2.5 3.2 4.3 0.5
25-20 16 9 5 4 11 14-15 25

+3.2 +2.5 +0.1 -0.8 -0.4 0.0 +0.2 -0.2 -1.3 -0.6 +0.6
5.4 6.1 8.5 9.4 9.0 8.6 8.4 8.8 9.2 9.2 8.0
25 18 14-12 10-8 5 5 10 13-14 15-16 18-25

+2.1 +1.3 -0.7 -1.6 -0.3 0.0 0.0 0.0 -0.6 -1.7 -0.4 -0.3 -1.1
35 43 63 7.2 5.9 5.6 5.6 6.2 7.3 6.0 5.9 6.7
25 19 14-12 11 10 5 3 5 10 14-15 17 21 25

+5.0 +4.0 +3.5 -1.9 -0.3 0.0 +0.2 -0.6 -1.7 +1.4
-1.5 -9.5 0.0 5.4 3.8 3.5 3.3 4.1 5.2 2.1
25 21 19 10-9 4 5 12 14-15 21-25

± Brown's Cor Rd.

50' Rt.

100' Rt.

25' Lt.

50' Lt.

Drain Lt ditch thru parallel pipe on Lt. Drain
Rt. ditch to East on Brown's Cor's Rd. ditch

allow Exc
+2.9 +1.7 -1.2 -0.1 0.0 -0.5 -1.0 +0.5 +1.6
3.1 4.3 7.2 6.1 6.0 6.5 7.0 5.5 4.4
25 17 12-11 9 9 14-15 13 25

Nail in brace pole Rt 15.9

10-24-'21
Fine

1178.70

160

- 8.5 70.2

+60

5.7 73.0

161

- 4.2 74.5

+25

3.6 75.1

B. M.

3.93 1174.73

162

- 5A 73.3

163

- 7.3 71.4

+50

8.7 70.0

T. F.
164

6.42 1175.78
9:34 1169.36
- 7.8 68.0

+50

9.9 65.9

Hanna
Gard
Thompson

33

+3.6 +2.8 -1.4 -0.7 0.0 -0.7 -1.7 +1.7 +2.3
4.9 5.7 10.1 9.2 8.5 9.2 10.2 6.6 6.2
25 20 13-12 9 9 9 13-15 20 25

+3.3 +3.1 -1.8 -0.6 0.0 -0.8 -2.0 +1.2 +1.3
2.4 2.6 7.5 6.3 5.7 6.5 7.7 4.5 4.4
25 18 13 9 9 10 13-14 15 25

+1.9 +1.3 -1.4 -0.4 0.0 -0.5 -1.2 +1.2 +1.1
2.3 2.2 5.6 4.6 4.2 4.7 5.4 3.0 3.1
25 18 14-13 9 9 9 13-14 17 25

+1.0 +0.9 +0.4 -1.8 -0.9 0.0 -0.4 -0.7 +1.1 +1.3
2.6 2.7 3.2 5.4 4.5 3.6 4.0 4.3 2.5 2.3
25 20 18 15-14 11 10 13 12 25

Staple in N.W. root 14" Maple, 25' Rt., 162 + 10

+1.4 +0.9 -2.0 -0.9 +0.1 0.0 -0.6 -1.3 -0.6 +1.5
4.0 4.5 7.4 6.3 5.3 5.4 6.0 6.7 6.0 3.9
25 18 14-13 10 2 8 12 14-15 22-25

-0.5 -0.6 -1.9 -0.8 0.0 -0.4 -1.3 -1.0 0.0
7.8 7.9 9.2 8.1 7.3 8.1 8.6 8.3 7.3
25 16 14-13 9 9 9 11-12 13 25

-0.9 -0.3 -1.8 -0.6 0.0 -0.3 -1.1 +0.2 +0.8
9.6 9.0 10.5 9.3 8.7 9.0 9.8 8.5 7.9
25 15 14-12 8 11 14-15 17 25

+0.3 +0.9 -1.9 -0.7 0.0 -0.6 -1.8 +3.3 +3.7
7.5 6.9 9.7 8.5 7.8 8.4 9.6 4.5 4.1
25 15 11-10 9 10 12-13 21 25

+1.7 +2.2 -2.0 -0.8 0.0 -1.0 -1.7 +4.5 +5.1
8.2 7.7 11.9 10.7 9.9 10.9 11.6 5.4 4.8
25-20 17 13-12 9 9 9 10-11 19 25

8
1175.78

165 - 11.8 64.0

T.P. 5.66 1169.62 11.82 1163.96
+50 7.6 62.0

166 - 11.0 58.6

+50 12.7 56.7

T.P. 2.64 1160.03 12.23 1157.39
167 - 5.7 54.6

+80 8.6 51.4

168 - 9.5 50.5

169 - 13.0 47.0

T.P. 2.22 1149.53 12.72 1147.31



+1.7 +2.0 -1.6 -0.8 0.0 -0.9 -1.5 +4.0 +4.5
10.1 9.8 13.4 12.6 11.8 12.7 13.3 7.8 7.3
25 17 12-11 9 9 9 11-12 20 25

-0.2 +0.4 +0.8 +1.2 -1.5 -0.7 0.0 -0.6 -1.6 +0.3 +2.8 +3.6
7.8 7.2 6.6 9.1 8.8 7.6 8.2 9.2 7.3 7.8 4.0
25 18 17-15 12-11 9 9 10 12-13 17 20 25

+1.4 +2.0 +2.7 -0.4 0.0 -0.5 -1.5 +2.4 +3.3 +5.2 +5.5
9.6 9.0 8.3 11.4 11.0 11.5 12.5 8.6 7.7 5.8 5.5
25 18 17-6 13 7 10-11 18 21 23 25

+2.2 +2.5 -1.5 -0.6 0.0 0.0 -1.0 -1.7 +4.7 +5.1
10.7 10.4 14.4 13.5 12.9 12.9 13.9 14.6 8.2 7.8
25 19 14-13 16 2 7 10-11 21 25

+1.5 +1.6 -0.7 -1.7 -0.8 +0.2 0.0 -0.7 -2.1 +3.1 +3.8 +4.1
3.9 3.8 9.1 7.1 6.2 5.2 5.4 6.1 7.5 2.3 1.6 1.3
25 22 17 16-15 12 3 7 9-10 18 22 25

-0.5 -0.7 -1.8 -0.7 0.0 -0.8 -1.9 -0.5 +2.6 +3.6
9.1 9.3 10.4 9.3 8.6 9.4 10.5 9.1 6.8 5.0
25 18 16-15 11 6 10-11 13-15 20 25

-0.2 -0.6 -2.1 -0.8 0.0 -0.9 -1.8 -0.3 +0.8
9.7 10.1 11.6 10.3 9.5 10.4 11.3 9.8 8.7
25 17 15-14 11 8 10-11 15 25

+1.3 +0.9 -1.8 -0.6 0.0 +0.2 -1.0 -1.8 +0.2 +0.5
11.7 12.1 14.8 13.6 13.0 12.8 14.0 14.8 13.3 12.5
25 16 12-11 7 A 13 15-16 20 25

1149.53

170 - 4.9 44.6

171 - 6.3 43.2

+90 9'-9" x 4'-0" 5.7 44.1

Good Cond

stone Abuts, Con. slab & H.W.s

Exc = (Cont of Abuts) x 2 Regd. Ext.

Point 150 Lin Ft.

Temp B.M. 4.95 || 44.58

7.44 42.09

11.7 37.8

7.43 42.10

11.5 38.0

5.0 44.5

172 - 5.2 44.3

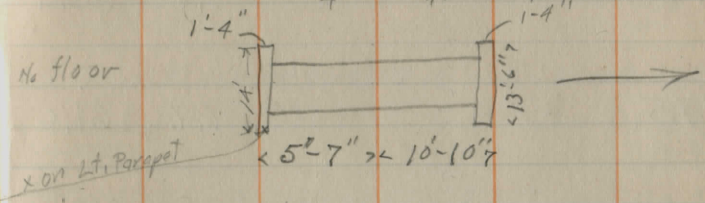
173 - 2.5 47.0

T.R 1104 1159 45 112 1148.41

+2.3 +1.9 -0.2 -1.7 -0.6 0.0 +0.1 -0.3 -1.1 -0.6 +0.6
2.6 3.0 5.1 6.6 5.5 7.9 4.8 5.2 6.0 5.5 4.3
2.5 2.3 1.9-1.3 1.1-1.0 2 4 10 14-16 17-20 25

-1.6 -0.7 -1.2 -0.3 0.0 +0.1 -0.2 -1.1 -0.7 -2.1
7.2 7.0 7.5 6.6 6.3 6.2 6.5 7.4 7.0 8.4
2.5 1.2 1.1-1.0 2 5 11 15-16 17 25

+0.2 0.0 +0.2 +0.4
5.2 5.7 5.7 5.0
4 9.5 Top.



Bot. of slab Lt.
Bot. creek Lt.
" of slab Rt.
" Creek Rt.
Top. Rt. parapet.

+2.9 -2.4 -1.7 -2.0 -3.9 -1.8 -0.1 0.0 0.0 -2.3 -1.0 -2.1
8.1 7.6 6.9 7.2 9.1 7.0 5.3 5.2 5.2 3.5 6.2 7.3
2.5 1.4 1.6 1.4 1.3-1.2 8 5 10 13-14 15 25

+3.1 +0.4 -1.7 -0.7 0.0 -0.6 -1.4 +0.7 +3.4
-0.6 2.1 4.2 3.2 2.5 3.1 3.9 1.8 -0.9
2.5 1.6-1.4 1.2 1.9 1.2 1.2 1.4-1.5 2.1 2.5

5
1159.75

+30 10.9 48.6

174 - 7.5 55.0

T.P. 9.39 1168 2.0 0.64 1158.81
+65 7.8 60.4

175 - 6.6 61.6

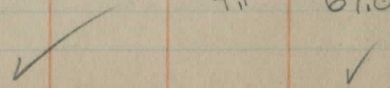
176 - 3.2 65.0

T.P. 5.16 1171.89⁹ 1.47 1166.73
177 - 3.7 68.2

+50 3.1 68.8

178 - 3.2 68.7

179 - 4.1 67.8



+5.9 +5.5 +1.3 -0.9 -0.3 0.0 -0.5 -1.5 +0.1 +5.4
50 54 9.6 14.8 11.2 10.8 11.4 12.4 10.8 5.5
30 25 18-16 14-13 11 11 14-15 17-19 25

+5.3 -0.6 -0.5 0.0 -0.1 -0.6 -2.2 +0.9 +6.7
-0.8 6.1 5.0 7.5 4.6 3.1 6.7 3.6 -2.2
25-24 15-14 10 8 12 14-15 18 26

+2.2 -2.2 -1.0 0.0 -0.6 -2.2 -0.8 +3.4
5.6 10.0 8.7 7.8 8.4 10.0 8.3 4.4
25-17 13-12 9 12 14-15 17-18 25

+1.8 +1.2 -2.0 -0.7 0.0 +0.1 -0.4 -1.8 -0.9 +2.0 +2.6
4.8 5.4 8.6 7.3 6.6 6.5 7.0 8.4 7.5 4.6 4.0
25 19 13-12 7 4 10 14-15 16-17 22 2.5

+2.8 -1.6 -0.9 0.0 -1.0 -1.7 -1.1 +2.0 +2.4
0.4 4.8 4.1 3.2 4.2 4.7 4.3 1.2 0.8
25-17 12-11 8 10 12-13 14-16 21 25

+1.1 +0.9 -1.6 -0.7 0.0 -0.4 -1.7 -0.4 +0.6
2.6 2.8 5.3 4.4 3.7 4.1 5.4 4.1 3.1
25 17 16-13 9 7 12-13 15 25

+0.5 -0.1 -1.2 -0.5 0.0 -0.5 -1.4 -0.9 -0.4
2.6 3.2 4.3 3.5 3.1 3.6 4.5 4.0 3.5
25 19 17-10 5 8 12-13 14 25

-0.5 -1.1 -1.5 -0.7 0.0 -0.6 -1.5 -1.0 -0.8
3.1 4.3 4.7 3.7 3.2 3.8 4.7 6.2 4.0
25 18-13 12 7 9 13-14 15 25

-0.2 -1.0 -0.8 -1.1 0.0 +0.4 -0.6 -1.4 -0.7 -1.1 -0.8
4.3 5.1 4.9 5.2 4.1 3.7 4.7 5.5 4.8 5.2 4.9
25 21 12 10 3 11 14-15 16 20 25

11 71 89

180 - 4.5 67.4

+55¢ 12" VP. Goods 4.5 67.4

(Reg. New cor. - Square up with new £.)

181 4.5 67.4

182 3.7 68.2

183 2.9 69.0

T.P. 5.98 1176 64 1.23 1170.66

B.M. 3.76 1176 57 3.76 1172.85

184 4.4 72.2

+25 3.4 73.2

185 5.0 71.6

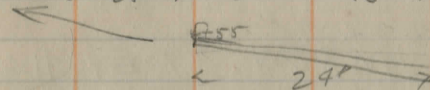
✓

LT & RT

31

-1.3 -0.8 -1.3 -0.6 0.0 +0.2 -0.5 -1.3 -0.9
 $\frac{5.8}{2.5}$ $\frac{5.3}{11}$ $\frac{5.8}{10-9}$ $\frac{5.1}{7}$ $\frac{4.5}{5}$ $\frac{4.3}{5}$ $\frac{5.0}{12}$ $\frac{5.8}{16-17}$ $\frac{5.4}{18-2.5}$

-3.6 -2.9 -2.5 -0.7 0.0 +0.1 -2.3 -0.6 -1.2
 $\frac{8.1}{7.5}$ $\frac{7.4}{2.5}$ $\frac{7.8}{10}$ $\frac{5.2}{9}$ $\frac{4.3}{5}$ $\frac{4.4}{13}$ $\frac{6.8}{15-16}$ $\frac{5.1}{19}$ $\frac{5.7}{2.5}$



-1.1 -0.9 -1.4 -0.6 0.0 +0.2 -0.3 -1.4 -0.6
 $\frac{5.6}{2.5}$ $\frac{5.4}{12}$ $\frac{5.9}{11-10}$ $\frac{5.1}{8}$ $\frac{4.5}{3}$ $\frac{4.3}{10}$ $\frac{4.8}{15-16}$ $\frac{5.9}{18-2.5}$

-0.6 -0.8 -1.1 -1.8 -0.9 0.0 -0.1 -0.8 -1.7 -0.9 -0.7
 $\frac{4.3}{2.8}$ $\frac{4.5}{15}$ $\frac{4.8}{4-12}$ $\frac{5.5}{11-10}$ $\frac{4.2}{7}$ $\frac{3.7}{6}$ $\frac{3.8}{2}$ $\frac{4.5}{11}$ $\frac{5.4}{14-15}$ $\frac{4.6}{12}$ $\frac{4.4}{2.5}$

+0.9 +0.4 -1.5 -0.5 0.0 +0.2 -0.4 -1.1 -0.2 +0.2
 $\frac{2.0}{2.5}$ $\frac{2.5}{13}$ $\frac{4.4}{10-9}$ $\frac{3.4}{5}$ $\frac{2.9}{5}$ $\frac{2.7}{4}$ $\frac{3.3}{10}$ $\frac{4.0}{13-14}$ $\frac{3.1}{15}$ $\frac{2.7}{2.5}$

Staple in E root P. Hickory, 30' LT, 183 + 40

+2.1 +1.6 +0.6 -0.7 -0.3 0.0 +0.4 -0.1 -0.7 +1.1 +1.6
 $\frac{2.3}{2.5}$ $\frac{2.8}{2.0}$ $\frac{3.8}{11}$ $\frac{5.1}{7}$ $\frac{4.7}{5}$ $\frac{4.4}{5}$ $\frac{4.0}{3}$ $\frac{4.5}{8}$ $\frac{5.1}{12-13}$ $\frac{3.3}{12}$ $\frac{2.8}{2.5}$

+1.2 +0.4 +0.9 -0.3 0.0 +0.2 -0.3 -0.9 +0.5 +0.7
 $\frac{2.2}{2.5}$ $\frac{3.0}{18}$ $\frac{2.5}{10}$ $\frac{3.7}{8}$ $\frac{3.4}{5}$ $\frac{3.2}{3}$ $\frac{3.7}{9}$ $\frac{4.3}{12}$ $\frac{2.9}{14}$ $\frac{2.7}{2.5}$

+0.6 +0.9 -0.6 -0.4 0.0 -0.2 -1.1 +1.4 +2.1
 $\frac{4.4}{2.5}$ $\frac{4.1}{14}$ $\frac{5.6}{11.4}$ $\frac{5.4}{7}$ $\frac{5.0}{5}$ $\frac{5.2}{7}$ $\frac{6.1}{10-11}$ $\frac{3.6}{15}$ $\frac{2.9}{2.5}$

1176⁶ 57

186

7.6 69.0

187

10.4 66.2

T.P. 1.94 1167.94

10.57 1166.00

188

4.8 63.1

+30

6.0 61.9

189

11.0 56.9

+50

13.6 54.3

T.P. 0.23 1155⁰ 78

12.39 1155.55

190

3.1 52.7

191

5.8 50.0

+86 & 2' x 1' stone Box.

7.5 48.3

Fair

Ret (2 x 2 or 14" deep) clean out (H) ✓

Lt,

←

Rt,

38

+1.2 +0.6 -0.9 -1.4 -0.8 0.0 0.0 -0.7 -1.6 -0.8 +1.0 +1.4
 $\frac{6.4}{25} \frac{7.0}{17} \frac{8.5}{15-14} \frac{9.0}{13} \frac{8.4}{12} \frac{7.6}{9} \frac{7.6}{2} \frac{8.3}{7} \frac{9.2}{10-11} \frac{8.1}{12-13} \frac{6.6}{16} \frac{6.2}{25}$

+0.6 0.0 -0.5 -1.9 -0.9 +0.1 0.0 -0.6 -1.7 +1.8 +1.4
 $\frac{9.8}{25} \frac{10.4}{24} \frac{10.9}{18} \frac{12.3}{16-15} \frac{11.3}{11} \frac{10.3}{3} \frac{10.4}{7} \frac{11.0}{7} \frac{12.1}{11-12} \frac{8.6}{17} \frac{2.0}{25}$

+1.0 +0.3 -0.5 -1.3 -0.6 0.0 -0.8 -1.8 -0.7 +1.2 +2.0
 $\frac{3.8}{25} \frac{4.5}{18} \frac{5.3}{14} \frac{6.1}{13-12} \frac{5.4}{9} \frac{4.8}{8} \frac{5.6}{8} \frac{6.6}{10-11} \frac{5.5}{12} \frac{3.6}{15} \frac{2.8}{20-25}$

-0.2 +0.2 -0.4 -2.5 -0.3 0.0 -0.5 -1.9 -0.6 +0.9 +2.2 +2.7
 $\frac{6.2}{25} \frac{5.8}{18} \frac{6.4}{13} \frac{8.5}{11} \frac{6.3}{7} \frac{6.0}{8} \frac{6.5}{10-11} \frac{7.9}{13} \frac{6.6}{17} \frac{5.1}{20} \frac{3.8}{25} \frac{3.3}{25}$

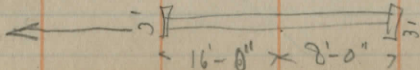
+3.0 -2.2 -1.0 -0.4 0.0 -0.2 -1.9 -0.8 +5.9 +6.7
 $\frac{8.0}{25} \frac{13.2}{17} \frac{12.0}{12-11} \frac{11.7}{9} \frac{11.0}{6} \frac{11.2}{9} \frac{12.9}{11-12} \frac{11.8}{13-14} \frac{5.1}{25} \frac{4.3}{30}$

+1.8 +6.4 -2.8 -0.5 0.0 -0.5 -1.4 -1.0 -0.5 +5.3 +6.9
 $\frac{11.8}{25} \frac{12.2}{18} \frac{15.4}{13-11} \frac{14.1}{8} \frac{13.6}{7} \frac{14.1}{7} \frac{15.0}{10-11} \frac{14.6}{12-15} \frac{14.1}{25} \frac{8.3}{25} \frac{7.2}{30}$

-0.2 -0.7 -1.3 -0.7 0.0 -0.5 -1.4 -1.1 -0.5 +2.8 +3.1
 $\frac{3.3}{25} \frac{3.8}{17} \frac{4.4}{16-12} \frac{3.8}{8} \frac{3.1}{6} \frac{3.6}{6} \frac{4.5}{9-10} \frac{4.2}{11} \frac{3.6}{18} \frac{3.3}{24} \frac{0.0}{25}$

-1.8 -0.9 -1.2 -0.5 0.0 -0.6 -1.2 -0.6 -0.3 0.0
 $\frac{7.6}{25} \frac{6.7}{15} \frac{7.0}{13-14} \frac{6.3}{10} \frac{5.8}{6} \frac{6.4}{6} \frac{7.0}{8-10} \frac{6.4}{11} \frac{6.1}{18} \frac{5.8}{25}$

-2.7 -2.5 +0.6 -0.2 0.0 -0.2 +1.0 -2.4 -2.8
 $\frac{10.2}{30} \frac{10.0}{17} \frac{4.9}{12} \frac{7.7}{15} \frac{7.5}{6} \frac{7.7}{7} \frac{4.5}{7} \frac{4.9}{8} \frac{10.3}{14-16}$



1155⁸78

192 7.8 48.0

193 8.8 47.0

194 8.9 46.9

B.M. 206 1153⁶59 42.9 1151.79+20 £ 12" C.I.P. (sec)
(fair cond) 6.5 47.1

195 6.5 47.1

196 5.5 48.1

+40 5.0 48.6

197 6.6 47.0

39

Lt.

£

Rt

-1.1	-1.1	-2.4	-0.6	0.0	0.0	-0.2	-2.1	-1.0	-0.4	-0.8
$\frac{83}{25}$	$\frac{89}{21}$	$\frac{102}{19}$	$\frac{87}{18}$	$\frac{78}{5}$	$\frac{78}{7}$	$\frac{80}{6}$	$\frac{99}{12}$	$\frac{88}{14}$	$\frac{82}{19}$	$\frac{86}{25}$

+0.1	-1.5	-0.9	+0.5	0.0	-0.1	-0.5	0.0	+1.6	+2.9
$\frac{87}{25}$	$\frac{103}{21}$	$\frac{97}{17}$	$\frac{83}{5}$	$\frac{88}{5}$	$\frac{89}{5}$	$\frac{93}{7}$	$\frac{88}{9}$	$\frac{72}{16}$	$\frac{59}{25}$

-0.9	-1.3	-1.9	-0.7	+0.1	0.0	-0.2	-1.5	-0.7	-0.1	-0.5	+0.2
$\frac{98}{25}$	$\frac{102}{23}$	$\frac{108}{22}$	$\frac{96}{18}$	$\frac{88}{10}$	$\frac{89}{4}$	$\frac{91}{4}$	$\frac{107}{9}$	$\frac{96}{11}$	$\frac{90}{12}$	$\frac{94}{14}$	$\frac{87}{25}$

staple in N.W. root 12" Walnut 30' Rt, 197

-2.9	-2.7	-0.5	+0.2	0.0	-0.1	-2.0	-1.9	-0.1
$\frac{94}{35}$	$\frac{92}{25}$	$\frac{70}{19}$	$\frac{63}{7}$	$\frac{65}{3}$	$\frac{66}{3}$	$\frac{85}{4}$	$\frac{84}{9}$	$\frac{66}{12}$

Gold fill RL, RL

<math>20'-6'' \times 3'-6''>

-0.7	-0.9	-0.1	+0.5	0.0	-1.0	-0.2	+1.4	+1.3	+2.5
$\frac{72}{25}$	$\frac{77}{22}$	$\frac{66}{16}$	$\frac{60}{8}$	$\frac{65}{8}$	$\frac{75}{5}$	$\frac{67}{8}$	$\frac{51}{14}$	$\frac{52}{18}$	$\frac{42}{25}$

-0.4	-0.9	-0.3	+0.6	0.0	-0.8	-0.1	+1.6	+2.9
$\frac{59}{25}$	$\frac{64}{23}$	$\frac{58}{16}$	$\frac{49}{7}$	$\frac{55}{7}$	$\frac{63}{4}$	$\frac{56}{7}$	$\frac{39}{12}$	$\frac{26}{25}$

-0.6	-1.0	-0.3	+0.6	0.0	-0.6	0.0	+2.2	+2.8
$\frac{56}{25}$	$\frac{60}{23}$	$\frac{53}{18}$	$\frac{44}{8}$	$\frac{50}{8}$	$\frac{56}{4}$	$\frac{50}{7}$	$\frac{28}{12}$	$\frac{22}{25}$

-0.8	-1.2	-0.1	+0.4	0.0	-1.2	+2.2	+3.2	+4.3
$\frac{74}{25}$	$\frac{78}{23}$	$\frac{67}{17}$	$\frac{62}{7}$	$\frac{66}{7}$	$\frac{78}{5}$	$\frac{44}{11}$	$\frac{34}{20}$	$\frac{23}{25}$

1153^c 59

198

10.0 43.6

199

13.9 39.7

T.P. ^{11:40 PM} 0.01 1142.45⁵

200

5.2 37.3

10-25-21
cloudy
50 mi gale
ce

201

7.8 34.7

202

10.7 31.8

T.P. 38.1 1133.96^{4.0}

203

12.31 1130.15
4.4 29.6

+65 \pm 1 1/2 x 1 1/2 stone box
Fair Condi.
Stone good for New H.W.

5.1 28.9

0.0 -0.6 -1.1 -0.1 +0.3 0.0 -1.5 +2.3 +3.2
100 106 111 101 97 100 115 77 68
25 22 21 20 15 7 6-7 14 25

-0.7 -1.1 -1.6 -0.4 +0.1 0.0 -1.5 -0.9 +1.4 +2.3
14.6 150 155 143 138 130 154 148 125 116
25 22 19 15 7 7-8 9-10 14 25

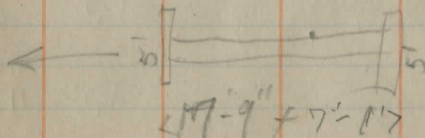
Tel. Pole Rt. 199 (rail E. side)
-0.5 -0.9 -1.2 -0.2 0.0 -0.3 -1.4 +0.2 +1.1
57 61 67 54 53 55 60 50 41
25 19 18 14 4 3-9 13 25

0.0 -0.8 -1.2 -1.9 -0.5 +0.2 0.0 -0.3 -1.3 +0.7 +1.4
78 84 90 97 83 76 78 81 91 71 64
25 22 19 18 17 14 4 3 6-9 12 25

+0.7 -1.1 -0.4 +0.1 0.0 -0.4 -1.4 -1.0 +1.9 +2.8
190 118 111 106 107 111 121 117 88 79
25 20 16 12 4 4 7-8 9-10 16 25

-0.7 -0.3 0.0 -0.1 -0.4 -0.2
51 47 44 45 48 46
25 14 5 8 25

-3.6 -2.6 -2.2 -0.2 +0.1 0.0 +0.1 -2.2 -2.0
87 77 73 57 50 51 50 73 71
50 25 18 16 6 6 8 25



1133¹⁰ 96

204 5.1 28.9

+50 4.4 29.6

+80 2.3 31.7

205 1.8 32.2

T.T. 5.37 1139² 6 0.17 1133.79
+15 6.3 32.9

+40 5.3 33.9

+75 4.1 35.1

206 4.3 34.9

B.M. 1134.78
A.36 1134.80

-0.6 -0.5 -0.7 -0.3 0.0 -0.3 -1.1 -0.3 +0.1
 $\frac{57}{25} \frac{56}{20} \frac{58}{17} \frac{54}{12} \frac{51}{5} \frac{54}{5} \frac{62}{9} \frac{54}{10} \frac{50}{25}$

-1.0 -0.4 0.0 0.0 -0.4 +0.1
 $\frac{54}{25} \frac{48}{24} \frac{48}{14} \frac{44}{14} \frac{48}{15} \frac{43}{22} \frac{43}{25}$

-1.8 0.0 -0.2 +0.1 -0.1
 $\frac{41}{25} \frac{23}{11} \frac{215}{11} \frac{22}{20} \frac{24}{25}$

-4.7 -2.3 0.0 +1.0 +0.9
Road $\frac{65}{50} \frac{41}{25} \frac{48}{18} \frac{38}{25} \frac{37}{50}$ Road

-2.8 -2.8 -3.7 -1.3 0.0 +1.7
 $\frac{91}{25} \frac{91}{21} \frac{100}{23} \frac{70}{12} \frac{63}{25} \frac{46}{25}$

+0.2 -0.8 -1.2 -1.7 -0.7 0.0 +0.7 +3.2 +4.0
 $\frac{51}{25} \frac{41}{20} \frac{65}{17} \frac{70}{16} \frac{60}{15} \frac{53}{10} \frac{46}{10} \frac{21}{25} \frac{12}{12}$
33 store porch

+1.2 -0.6 -1.0 -0.6 0.0 +0.5 +1.9
 $\frac{29}{25} \frac{47}{20} \frac{51}{16} \frac{47}{10} \frac{41}{10} \frac{36}{13} \frac{22}{25}$

+0.6 -0.5 0.0 0.0 +0.1 +2.0 +2.2
 $\frac{37}{25} \frac{48}{17} \frac{43}{12} \frac{43}{14} \frac{42}{16} \frac{23}{22} \frac{21}{25}$

Staple in S.E. root 10" Maple 30'lt. 206+27

11:39² 16

207 4.7 34.5

5' + E 10" V.I.P. 4.4 34.6

12" Pipe Regd.,
Bring water in E ditch back from store

208 4.4 34.8

209 3.4 35.8

T.P. 10.07 11.45 4.4 3.79 1135.37

210 7.5 37.9

211 5.6 39.8

+60 4.3 41.1

212 3.0 42.4

+15 2.7 42.7

-2.1 -1.0 -1.4 -0.8 -0.1 0.0 -0.5 -1.5 -0.8 -0.5 +0.4 +1.2
6.8 5.7 6.1 5.5 4.8 4.7 5.2 6.2 5.5 5.2 3.7 3.5
2.5 15 14 10 3 8 11 12 13 14 15 22 25

-3.6 -2.9 -0.9 0.0 -0.5 -2.7 -2.0 -0.4 +0.5
8.2 7.5 5.5 4.6 5.1 7.3 6.5 5.0 4.1
14 11 8 10 13 15 25
←

part broken
x 13' x 9'-6"

-1.6 -1.0 -1.2 -0.6 0.0 -0.6 -1.5 -0.7 +0.8
6.0 5.4 5.2 5.0 4.4 5.0 5.9 5.1 3.6
2.5 14 13 9 8 11 12 15 18 25

-0.5 -0.9 -0.8 -1.2 -0.6 0.0 -0.7 -1.1 -0.4 +1.8 +2.5
3.9 4.3 4.2 4.6 4.0 3.4 4.1 4.5 3.8 1.6 0.9
2.5 21 13 12 11 7 10 13 15 16 22 25

-1.1 -1.2 -1.8 -0.7 0.0 -0.3 -1.8 -0.2 +1.0
8.6 8.7 9.3 8.2 7.5 7.8 9.3 7.7 6.5
2.5 14 15 12 7 7 12 14 17 25

-0.1 -0.8 -1.7 -0.8 0.0 -0.5 -1.5 -0.9 +0.6 +1.4
5.7 6.4 7.3 6.4 5.6 6.1 7.1 6.5 5.0 4.2
2.5 17 15 14 8 7 12 13 14 15 19 25

+1.5 0.0 -0.3 -1.7 -0.8 0.0 0.0 -0.9 -1.5 +1.2 +2.6
4.8 4.3 4.6 6.0 5.1 4.3 4.3 5.2 5.8 3.1 1.7
2.5 20 17 15 14 9 2 10 12 13 17 25

+0.6 0.0 -1.7 -0.7 0.0 -0.4 -1.5 +0.9 +1.9
2.4 3.0 4.7 3.7 3.0 3.4 4.5 2.1 1.1
2.5 23 18 15 14 9 8 13 14 18 25

same as 212

114544

213

5.3 40.1

+1.0	+0.1	-1.7	-0.7	+0.1	0.0	-0.7	-1.6	+1.4	+2.7
<u>4.3</u>	<u>5.2</u>	<u>7.0</u>	<u>6.0</u>	<u>5.2</u>	<u>5.3</u>	<u>6.0</u>	<u>6.9</u>	<u>3.9</u>	<u>2.9</u>
25	18	16-15	10	2		9	14-15	19	25

214

7.0 38.4

-1.3	-1.1	-1.6	-0.9	0.0	-1.1	-2.0	-1.1	-0.4	0.0
<u>8.3</u>	<u>8.1</u>	<u>8.6</u>	<u>7.9</u>	<u>7.0</u>	<u>8.1</u>	<u>9.0</u>	<u>8.1</u>	<u>7.4</u>	<u>7.0</u>
25	14	13-12	7		11	14-15	16	20	25

T.P. 1141 73 7.98 1137.6

214 90° tile Reg. 12" pipe 4.6 37.1

-3.7	-3.4	-1.4	-0.2	0.0	-0.3	-2.4	-1.4	-1.0
<u>8.3</u>	<u>8.0</u>	<u>6.0</u>	<u>4.8</u>	<u>4.6</u>	<u>4.9</u>	<u>7.0</u>	<u>6.0</u>	<u>5.6</u>
25	14	13	8		10	11-14	15	25

215

4.8 36.9

-2.0	-1.5	-2.2	-0.4	0.0	-0.1	-2.3	-0.9	-0.8
<u>6.8</u>	<u>6.4</u>	<u>7.0</u>	<u>5.2</u>	<u>4.8</u>	<u>4.9</u>	<u>7.1</u>	<u>5.7</u>	<u>5.6</u>
25	19	18-15	10		9	13-14	16	25

216

4.4 37.3

-0.2	0.0	-1.2	-0.5	0.0	-0.9	+0.6	+1.6
<u>4.6</u>	<u>4.4</u>	<u>5.6</u>	<u>4.9</u>	<u>4.4</u>	<u>5.3</u>	<u>3.8</u>	<u>2.8</u>
25	16	14-13	9		10	12	25

+25

4.1 37.6

+0.7	-0.1	-1.4	-0.6	0.0	-0.3	-1.0	+1.2	+2.0
<u>3.4</u>	<u>4.2</u>	<u>5.5</u>	<u>4.7</u>	<u>4.1</u>	<u>4.4</u>	<u>5.1</u>	<u>2.9</u>	<u>2.1</u>
25	6	14-13	9		4	9	13	25

B.M.

2.03 1139.64

Staple in N.W. root 12" Maple 30' Rt. 215+85

217

7.7 34.0

+2.5	+0.9	-1.3	-0.4	+0.1	0.0	-0.6	-1.5	+0.9	+1.9	+2.6
<u>5.2</u>	<u>6.8</u>	<u>9.0</u>	<u>8.1</u>	<u>7.6</u>	<u>7.7</u>	<u>8.3</u>	<u>4.2</u>	<u>6.8</u>	<u>5.8</u>	<u>5.1</u>
25	18	16-15	12	3		6	9-10	13	21	25

218

13.7 28.0

-0.6	-1.5	-0.5	+0.2	0.0	-0.3	-1.3	+1.2	+2.0
<u>14.3</u>	<u>5.2</u>	<u>14.2</u>	<u>13.5</u>	<u>13.7</u>	<u>14.0</u>	<u>15.0</u>	<u>12.5</u>	<u>11.7</u>
12.0	15-14	10	2		7	11-12	16	25

T.P. 1129 36 12.55 1129.18

1129 36

219

6.3 23.1

220

12.4 17.0

T.P. 0.32 1117 03

12.65 1116.71

221

6.3 10.2

222

11.7 05.3

T.P. ^{PM} 0.64 1105 24

12.43 1104.60

223

3.0 02.2

224

5.8 99.4

225

8.4 96.8

T.P. 1.93 1097 83

9.3A 1095.90

B.M.

1.62 1096.20
1096.12

226

3.7 94.1

44

$$\begin{array}{cccccccccccc} +2.3 & +1.9 & -2.1 & -0.4 & +0.1 & 0.0 & -0.9 & -2.5 & -0.5 & +0.9 & +2.0 \\ \frac{4.0}{25} & \frac{4.9}{20} & \frac{8.4}{15} & \frac{6.7}{10} & \frac{6.2}{2} & \frac{6.3}{7} & \frac{7.2}{10} & \frac{8.8}{11} & \frac{6.8}{13} & \frac{5.1}{16} & \frac{4.3}{25} \end{array}$$

$$\begin{array}{cccccccccccc} +2.5 & +2.1 & -0.6 & -2.5 & -0.3 & 0.0 & -0.5 & -2.6 & +2.7 & +3.2 \\ \frac{9.9}{25} & \frac{10.3}{23} & \frac{13.0}{19} & \frac{14.9}{17} & \frac{12.7}{11} & \frac{12.4}{7} & \frac{12.9}{7} & \frac{15.0}{12} & \frac{9.7}{13} & \frac{9.2}{25} \end{array}$$

$$\begin{array}{cccccccccccc} +2.8 & -0.6 & -1.6 & -0.5 & +0.1 & 0.0 & -0.8 & -2.3 & -1.2 & +3.8 & +4.7 \\ \frac{4.0}{25} & \frac{7.4}{24} & \frac{8.4}{19} & \frac{7.3}{13} & \frac{6.7}{3} & \frac{6.8}{8} & \frac{7.6}{11} & \frac{9.1}{12} & \frac{8.0}{13} & \frac{3.0}{20} & \frac{2.1}{25} \end{array}$$

$$\begin{array}{cccccccccccc} +1.7 & +1.3 & -0.7 & -1.4 & -0.5 & +0.3 & 0.0 & -0.4 & -1.6 & -0.8 & +2.7 & +3.4 \\ \frac{4.0}{25} & \frac{10.7}{24} & \frac{12.4}{21} & \frac{13.1}{16} & \frac{12.7}{15} & \frac{11.4}{12} & \frac{11.7}{3} & \frac{12.1}{5} & \frac{13.3}{9} & \frac{12.5}{10} & \frac{9.0}{11} & \frac{8.3}{12} \end{array}$$

$$\begin{array}{cccccccccccc} -0.4 & -0.3 & -1.9 & -0.3 & +0.2 & 0.0 & -0.4 & -1.7 & -0.3 & +0.3 \\ \frac{3.4}{25} & \frac{3.3}{20} & \frac{4.9}{12} & \frac{3.3}{10} & \frac{2.8}{3} & \frac{3.0}{7} & \frac{3.4}{6} & \frac{4.7}{11} & \frac{3.3}{12} & \frac{2.7}{15} \end{array}$$

$$\begin{array}{cccccccccccc} -0.5 & -0.2 & -1.5 & -0.2 & 0.0 & -0.4 & -1.4 & -0.6 & -0.7 \\ \frac{6.3}{25} & \frac{6.0}{19} & \frac{7.3}{15} & \frac{6.0}{9} & \frac{5.8}{7} & \frac{6.2}{11} & \frac{7.2}{12} & \frac{6.4}{14} & \frac{6.5}{25} \end{array}$$

$$\begin{array}{cccccccccccc} +0.3 & -1.1 & -2.0 & -1.0 & 0.0 & -1.0 & -2.0 & -0.2 & -0.4 \\ \frac{9.1}{25} & \frac{9.5}{16} & \frac{10.7}{14} & \frac{9.4}{11} & \frac{8.4}{8} & \frac{9.4}{10} & \frac{10.4}{12} & \frac{8.6}{13} & \frac{8.8}{25} \end{array}$$

Staple in Eirroot 12' ^{Elm} ~~Maple~~ 85' Lt. 22575
 MADE OK

$$\begin{array}{cccccccccccc} +1.1 & +0.7 & -1.2 & -0.4 & 0.0 & -0.3 & -1.0 & -0.4 & -0.2 & +1.0 & +1.3 \\ \frac{2.0}{25} & \frac{3.0}{21} & \frac{4.9}{12} & \frac{4.1}{10} & \frac{3.7}{5} & \frac{4.0}{8} & \frac{4.7}{13} & \frac{4.1}{14} & \frac{3.7}{17} & \frac{2.7}{19} & \frac{3.4}{23} \end{array}$$

1097.83

227 5.2 92.6

228 6.5 91.3

229 7.6 90.2

T.P. 1.49 1091.09 8.23 1089.60

+55¢ 12" K.P. 1.3 89.8

230 2.2 88.9

231 3.5 87.6

232 5.2 85.9

233 6.2 84.9

45

$$\begin{array}{cccccccc} -1.0 & -0.7 & -1.4 & -0.5 & 0.0 & -0.3 & -0.9 & -0.6 \\ \frac{6.2}{2.5} & \frac{5.9}{12} & \frac{6.6}{11-10} & \frac{5.7}{6} & \frac{5.2}{8} & \frac{5.5}{8} & \frac{6.1}{13-12} & \frac{5.8}{14-2.5} \end{array}$$

$$\begin{array}{cccccccc} -0.8 & -0.7 & -1.4 & -0.4 & 0.0 & -0.3 & -1.1 & -0.5 & -1.5 \\ \frac{7.3}{2.5} & \frac{7.2}{12} & \frac{7.9}{11-10} & \frac{6.9}{6} & \frac{6.5}{8} & \frac{6.8}{8} & \frac{7.6}{12-13} & \frac{7.0}{15-15} & \frac{8.0}{2.5} \end{array}$$

$$\begin{array}{cccccccc} -0.5 & -1.4 & -0.2 & 0.0 & -0.4 & -1.2 & -0.3 & -1.5 & -1.7 \\ \frac{8.1}{2.5-1.4} & \frac{9.0}{12-11} & \frac{7.8}{6} & \frac{7.6}{8} & \frac{8.0}{8} & \frac{8.8}{11-13} & \frac{7.9}{14-17} & \frac{9.1}{20} & \frac{9.3}{2.5} \end{array}$$

$$\begin{array}{cccccccc} -0.8 & -1.2 & -1.5 & -0.6 & 0.0 & -0.1 & -1.6 & -1.5 & -3.1 \\ \frac{2.1}{2.5} & \frac{1.5}{7.5} & \frac{2.8}{13-10} & \frac{1.9}{9} & \frac{1.3}{13} & \frac{1.4}{7} & \frac{2.7}{11-12} & \frac{2.8}{2.5} & \frac{4.4}{7.5} \end{array}$$

$$\begin{array}{cccccccc} -0.5 & -0.9 & -1.6 & -0.1 & 0.0 & -0.7 & -1.6 & -0.8 & -0.9 \\ \frac{2.7}{2.5} & \frac{3.1}{14} & \frac{3.8}{13-12} & \frac{2.3}{3} & \frac{2.2}{7} & \frac{2.9}{7} & \frac{3.8}{11-12} & \frac{3.0}{14} & \frac{3.1}{2.5} \end{array}$$

$$\begin{array}{cccccccc} +0.4 & -0.3 & -0.6 & -0.5 & 0.0 & +0.1 & -0.4 & -1.6 & -1.0 & -0.3 & +0.2 \\ \frac{3.1}{2.5} & \frac{3.8}{17} & \frac{5.1}{15-14} & \frac{4.0}{8} & \frac{3.5}{2} & \frac{3.7}{7} & \frac{5.1}{12-13} & \frac{4.5}{14-15} & \frac{3.8}{18} & \frac{3.3}{2.5} \end{array}$$

$$\begin{array}{cccccccc} +0.8 & +0.4 & -1.0 & -1.7 & -0.5 & 0.0 & -0.6 & -1.4 & +0.3 & +1.1 \\ \frac{4.8}{2.5} & \frac{1.3}{14} & \frac{6.2}{16-15} & \frac{6.9}{14-13} & \frac{5.7}{6} & \frac{5.2}{9} & \frac{5.8}{9} & \frac{6.6}{12-13} & \frac{4.9}{15} & \frac{9.1}{2.5} \end{array}$$

$$\begin{array}{cccccccc} 0.0 & -0.4 & -1.0 & -1.7 & -0.5 & 0.0 & -0.7 & -1.2 & -0.6 & +0.1 \\ \frac{6.2}{2.5} & \frac{6}{14} & \frac{7.2}{14} & \frac{7.9}{15-13} & \frac{6.7}{9} & \frac{6.2}{9} & \frac{6.9}{2} & \frac{7.4}{12-13} & \frac{6.8}{13-14} & \frac{6.1}{15-2.5} \end{array}$$

1091 09

234 72 83.9

235 78 83.3

T.F. 3.65 1085 9.1 883 1082.26
236 3.0 82.9

237 3.4 82.5

238 4.0 81.9

239 5.0 80.9

240 5.41 1085 82 5.41 1089.50
7.12 78.6

241 8.2 77.6

T.F. 235 1078 6.0 957 1076.25

46

$$\begin{array}{cccccccc} -0.2 & -0.6 & -1.4 & -0.9 & 0.0 & -0.5 & -1.3 & -1.0 & -0.4 \\ \frac{7.4}{25} & \frac{7.8}{16} & \frac{8.6}{15-14} & \frac{8.1}{12} & \frac{7.2}{6} & \frac{7.7}{6} & \frac{8.5}{10-11} & \frac{8.2}{12-14} & \frac{7.6}{16-25} \end{array}$$

$$\begin{array}{cccccccc} -0.7 & -0.8 & -1.4 & -0.6 & +0.1 & 0.0 & -0.5 & -1.2 & -0.9 & -1.2 \\ \frac{8.5}{25} & \frac{8.6}{15} & \frac{9.2}{14-13} & \frac{8.4}{12} & \frac{7.7}{3} & \frac{7.8}{7} & \frac{8.3}{7} & \frac{8.0}{10-11} & \frac{8.7}{12} & \frac{8.0}{25} \end{array}$$

$$\begin{array}{cccccccc} -0.7 & -0.8 & -1.5 & -0.6 & 0.0 & -0.6 & -1.6 & -1.0 & -1.4 \\ \frac{3.7}{25} & \frac{3.8}{15} & \frac{4.5}{14-13} & \frac{3.6}{9} & \frac{3.0}{9} & \frac{3.6}{8} & \frac{4.6}{11-12} & \frac{4.0}{14} & \frac{4.4}{25} \end{array}$$

$$\begin{array}{cccccccc} -0.3 & -0.6 & -1.5 & -0.8 & 0.0 & -0.9 & -1.7 & -1.1 \\ \frac{3.7}{25} & \frac{4.0}{14} & \frac{4.9}{13-12} & \frac{4.2}{9} & \frac{3.4}{9} & \frac{4.3}{11} & \frac{5.1}{13-14} & \frac{4.5}{15-25} \end{array}$$

$$\begin{array}{cccccccc} -0.4 & -0.8 & -1.9 & -1.0 & 0.0 & 0.0 & -0.8 & -1.7 & -0.9 \\ \frac{4.4}{25} & \frac{4.8}{15} & \frac{5.9}{15-12} & \frac{5.0}{9} & \frac{4.0-4.8}{2} & \frac{4.8}{12} & \frac{5.7}{14-15} & \frac{4.9}{12} & -2.5 \end{array}$$

$$\begin{array}{cccccccc} +0.7 & +0.1 & -1.7 & -2.3 & -0.8 & 0.0 & -0.7 & -2.3 & -0.1 & +0.7 \\ \frac{4.3}{25} & \frac{4.9}{18} & \frac{6.7}{15-14} & \frac{7.3}{13-12} & \frac{5.8}{8} & \frac{5.0}{8} & \frac{5.7}{11} & \frac{7.3}{15-16} & \frac{5.1}{19} & \frac{4.3}{25} \end{array}$$

Staple S. Erroot 12" W. Sherry, 30'K+ 240.10

$$\begin{array}{cccccccc} +1.8 & +1.2 & -0.6 & -1.4 & -0.7 & 0.0 & -0.5 & -1.4 & +0.7 & +1.2 \\ \frac{5.4}{25} & \frac{6.0}{18} & \frac{7.8}{15} & \frac{8.6}{11-10} & \frac{7.9}{6} & \frac{7.2}{6} & \frac{7.7}{6} & \frac{8.6}{13-14} & \frac{6.5}{18} & \frac{6.9}{25} \end{array}$$

$$\begin{array}{cccccccc} -1.5 & -0.5 & -1.3 & -0.6 & 0.0 & +0.3 & -0.4 & -1.2 & -0.6 & -0.8 \\ \frac{9.7}{25} & \frac{8.7}{17-12} & \frac{9.5}{11-10} & \frac{8.3}{7} & \frac{8.1}{3} & \frac{7.9}{6} & \frac{8.6}{6} & \frac{9.4}{12-13} & \frac{8.8}{14} & \frac{9.0}{25} \end{array}$$

1078 60

242

2.5 76.1

243

3.6 75.0

244

5.1 73.5

+80E 10" V.P.
(12" Reg'd)

5.0 73.6

245

4.8 73.8

246

3.0 75.6

T.P.
+80

689

1083

1.7

232 1076.28

3.3 79.9

247

4.2 79.0

47

-0.6	-0.1	-0.8	-1.9	-0.9	0.0	-0.6	-1.3	-0.7	+0.4	+0.8
$\frac{3.1}{25}$	$\frac{2.4}{15}$	$\frac{3.3}{12}$	$\frac{4.4}{11}$	$\frac{3.4}{8}$	$\frac{2.9}{8}$	$\frac{3.1}{7}$	$\frac{3.8}{10}$	$\frac{3.2}{12}$	$\frac{2.1}{14}$	$\frac{1.7}{16}$

-1.2	-1.0	-2.0	-1.0	0.0	-0.6	-1.5	-1.0	0.0
$\frac{4.8}{25}$	$\frac{4.6}{14}$	$\frac{5.4}{13}$	$\frac{4.5}{12}$	$\frac{3.6}{9}$	$\frac{4.2}{6}$	$\frac{5.1}{10}$	$\frac{4.6}{12}$	$\frac{5.0}{12}$

+0.6	+0.9	-0.8	-1.2	-0.9	0.0	-0.3	-1.0	+0.2	+0.7
$\frac{4.5}{25}$	$\frac{4.2}{20}$	$\frac{5.9}{17}$	$\frac{6.3}{15}$	$\frac{6.0}{13}$	$\frac{5.1}{10}$	$\frac{5.4}{6}$	$\frac{6.1}{10}$	$\frac{4.9}{13}$	$\frac{4.4}{25}$

-3.3	-1.0	0.0	-0.8	-2.5	-2.3	-1.0	-1.3
$\frac{8.3}{20}$	$\frac{6.0}{18}$	$\frac{5.0}{16}$	$\frac{5.8}{11}$	$\frac{7.5}{13}$	$\frac{7.3}{15}$	$\frac{6.0}{16}$	$\frac{6.3}{25}$

inlet
12" V.P. pipe
sewer

30'

-1.7	-1.4	-2.6	-0.6	0.0	-0.6	-1.8	-0.9	-1.1
$\frac{6.5}{25}$	$\frac{6.3}{19}$	$\frac{7.4}{18}$	$\frac{5.4}{17}$	$\frac{4.7}{12}$	$\frac{5.4}{8}$	$\frac{6.5}{11}$	$\frac{5.7}{13}$	$\frac{5.3}{25}$

+1.7	+1.6	-0.3	-1.1	0.0	0.0	-0.3	-0.8	+0.3	+1.2
$\frac{1.3}{25}$	$\frac{1.4}{24}$	$\frac{3.3}{18}$	$\frac{4.1}{14}$	$\frac{3.0}{3}$	$\frac{3.0}{3}$	$\frac{3.8}{10}$	$\frac{2.7}{11}$	$\frac{1.8}{14}$	$\frac{1.8}{25}$

+1.4	-0.3	0.0	-0.7	+1.1	+1.4
$\frac{1.9}{25}$	$\frac{3.6}{10}$	$\frac{3.3}{3}$	$\frac{4.0}{10}$	$\frac{2.2}{12}$	$\frac{1.9}{25}$

+1.9	+1.0	0.0	-0.6	0.0	-0.4	+1.2	+2.3
$\frac{2.3}{25}$	$\frac{3.2}{16}$	$\frac{4.2}{14}$	$\frac{4.8}{10}$	$\frac{4.2}{7}$	$\frac{4.6}{10}$	$\frac{3.0}{12}$	$\frac{1.9}{25}$

1083 L7

248

8.1 75.1

249

10.2 73.0

T.P. 388 1076 20

10.85 1072.32
250 3.8 72.4

251

4.6 71.6

+75 £ 2 x 1/2 Stone box, 4.6 71.6
fair Cond.
Ext. Rt. end use Top Cap Stone.

252

4.8 71.4

253

4.5 71.7

+15

4.5 71.7

B.M.

2.63 73.56
1073.57

48

$$\begin{array}{cccccccccccc} +1.5 & +0.9 & +0.8 & -1.2 & -0.7 & 0.0 & 0.0 & -0.5 & -1.1 & +1.0 & +1.4 \\ \frac{6.6}{25} & \frac{7.2}{19} & \frac{7.3}{14} & \frac{9.3}{10.9} & \frac{8.8}{7} & \frac{8.1}{4} & \frac{8.1}{9} & \frac{8.6}{12-13} & \frac{9.2}{19} & \frac{7.1}{19} & \frac{6.7}{25} \end{array}$$

$$\begin{array}{cccccccc} -1.7 & -1.5 & -0.7 & -1.0 & 0.0 & -0.8 & -1.0 \\ \frac{11.9}{25} & \frac{11.7}{17} & \frac{10.9}{11} & \frac{11.2}{10} & \frac{10.2}{13} & \frac{11.0}{13} & \frac{11.2}{25} \end{array}$$

$$\begin{array}{cccccccc} -0.8 & -1.0 & -1.5 & 0.0 & -0.9 & -1.6 & -0.9 & -0.6 \\ \frac{4.6}{25} & \frac{4.8}{14} & \frac{5.3}{17} & \frac{3.8}{10} & \frac{4.7}{10} & \frac{5.4}{13-14} & \frac{4.7}{15} & \frac{4.4}{18-25} \end{array}$$

$$\begin{array}{ccccccccccc} -0.6 & -0.7 & -1.4 & -0.6 & 0.0 & -1.0 & -1.9 & -1.0 & +0.3 & +1.1 \\ \frac{5.2}{25} & \frac{5.3}{15} & \frac{6.0}{14-13} & \frac{5.2}{9} & \frac{4.6}{10} & \frac{5.6}{10} & \frac{6.5}{12-13} & \frac{5.6}{14} & \frac{4.3}{20} & \frac{3.5}{25} \end{array}$$

$$\begin{array}{cccccccc} -2.6 & -0.7 & 0.0 & +0.1 & -2.2 & -2.2 & -1.1 \\ \frac{7.2}{15} & \frac{4.8}{12} & \frac{4.6}{8} & \frac{4.5}{8} & \frac{6.8}{11} & \frac{6.8}{17} & \frac{6.7}{18-21} & \frac{5.7}{25} \end{array}$$

14'-0" x 10'-6"

$$\begin{array}{ccccccccccc} -1.3 & -2.2 & -1.0 & -0.4 & +0.1 & 0.0 & -0.3 & -1.6 & -0.7 & +0.3 \\ \frac{6.1}{25-23} & \frac{7.0}{22-21} & \frac{5.8}{19} & \frac{5.2}{13} & \frac{4.7}{3} & \frac{4.8}{3} & \frac{5.1}{9} & \frac{6.4}{11-12} & \frac{5.5}{13-20} & \frac{4.5}{25} \end{array}$$

$$\begin{array}{cccccccc} -0.6 & -0.5 & -1.0 & +0.5 & 0.0 & -0.3 & +0.1 & +0.1 \\ \frac{5.1}{25} & \frac{5.0}{20} & \frac{5.5}{17} & \frac{4.0}{5} & \frac{4.5}{5} & \frac{4.8}{5} & \frac{4.1}{10} & \frac{4.4}{25} \end{array}$$

$$\begin{array}{cccccccc} -0.1 & -0.2 & -0.8 & -0.1 & +0.6 & 0.0 & -0.3 & +1.5 & +2.6 & +3.1 \\ \frac{4.6}{25} & \frac{4.7}{20} & \frac{5.3}{17} & \frac{4.6}{13} & \frac{3.9}{7} & \frac{4.5}{7} & \frac{4.8}{6} & \frac{3.0}{11} & \frac{1.9}{13} & \frac{1.4}{25} \end{array}$$

Spike in S.W. foot 14" Maple 27' Rt. 2527 80

1076 20

+65

3.4 72.8

254

4.3 71.9

+79 ± 10" K.P.
(Reqd 18")

4.6 71.6

255

4.8 71.4

256

4.0 72.2

T.P. 12.10 1085 54

2.76 1073.44
257 12.3 73.2

258

10.7 74.8

259

9.4 76.1

$$\begin{array}{r} -0.7 -0.4 -1.0 +0.3 +0.4 0.0 -0.6 +1.9 +3.9 \\ \frac{4.1}{25} \quad \frac{3.7}{20} \quad \frac{4.4}{18} \quad \frac{3.7}{13} \quad \frac{3.0}{5} \quad \frac{3.4}{7} \quad \frac{4.0}{7} \quad \frac{1.5}{13} \quad \frac{-0.5}{25} \end{array}$$

$$\begin{array}{r} -0.2 +0.1 -0.7 0.0 +0.6 0.0 -0.6 +2.6 +3.9 \\ \frac{4.5}{25} \quad \frac{4.2}{21} \quad \frac{5.0}{18} \quad \frac{4.3}{14} \quad \frac{3.7}{7} \quad \frac{4.3}{7} \quad \frac{4.9}{8} \quad \frac{1.7}{15} \quad \frac{0.7}{25} \end{array}$$

$$\begin{array}{r} -2.9 -2.7 -1.6 -0.3 0.0 -0.6 -1.7 -1.7 -0.3 \\ \frac{7.5}{25} \quad \frac{7.3}{19} \quad \frac{6.2}{17.5} \quad \frac{4.9}{13} \quad \frac{4.8}{7} \quad \frac{5.7}{7} \quad \frac{6.3}{21} \quad \frac{6.3}{11} \quad \frac{4.9}{25} \end{array}$$

good fall

$$\begin{array}{r} -1.4 -1.5 -0.7 -1.6 -0.5 0.0 0.0 -0.1 -1.2 -0.3 -0.1 \\ \frac{6.4}{25} \quad \frac{6.3}{21} \quad \frac{5.5}{17} \quad \frac{6.4}{15} \quad \frac{5.3}{14} \quad \frac{4.8}{12} \quad \frac{4.8}{7} \quad \frac{4.9}{7} \quad \frac{6.9}{8} \quad \frac{5.1}{10} \quad \frac{4.9}{25} \end{array}$$

$$\begin{array}{r} -1.1 -0.6 -1.1 -0.5 +0.2 0.0 -0.6 -1.1 -0.4 +0.6 +1.6 \\ \frac{5.1}{25} \quad \frac{4.6}{16} \quad \frac{5.1}{14} \quad \frac{4.5}{13} \quad \frac{3.8}{10} \quad \frac{4.0}{7} \quad \frac{4.5}{5} \quad \frac{5.1}{9} \quad \frac{4.4}{10} \quad \frac{3.4}{12} \quad \frac{2.4}{14} \quad \frac{2.4}{25} \end{array}$$

$$\begin{array}{r} -0.8 -0.7 -1.3 -0.7 +0.2 0.0 -0.4 -1.1 -0.4 -0.6 -0.4 \\ \frac{13.1}{25} \quad \frac{13.0}{16} \quad \frac{13.5}{15} \quad \frac{13.0}{14} \quad \frac{12.1}{7} \quad \frac{12.3}{7} \quad \frac{12.7}{5} \quad \frac{13.4}{9} \quad \frac{12.7}{11} \quad \frac{12.9}{10} \quad \frac{12.7}{25} \end{array}$$

$$\begin{array}{r} -0.1 -0.9 -1.5 -0.9 +0.1 0.0 -0.4 -1.2 -0.6 -0.2 \\ \frac{10.8}{25} \quad \frac{11.6}{16} \quad \frac{12.2}{15} \quad \frac{11.6}{13} \quad \frac{10.6}{3} \quad \frac{10.7}{7} \quad \frac{11.8}{4} \quad \frac{11.7}{8} \quad \frac{10.3}{10} \quad \frac{10.9}{25} \end{array}$$

$$\begin{array}{r} +1.4 +1.1 -1.6 -0.6 +0.2 0.0 -0.7 -1.3 -0.5 +0.4 \\ \frac{8.0}{25} \quad \frac{8.3}{21} \quad \frac{14.0}{16} \quad \frac{10.0}{11} \quad \frac{9.2}{4} \quad \frac{0.4}{7} \quad \frac{10.1}{7} \quad \frac{10.7}{9} \quad \frac{9.9}{11} \quad \frac{9.0}{25} \end{array}$$

1085 54

260

7.5

78.0

+75 End of Con.

5.3

80.2

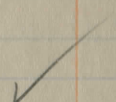
B.M.

0.79

1084.75

3.1

82.4



50

+1.9	+1.7	-0.6	-1.4	-1.0	+0.3	0.0	-0.6	-1.7	+0.1	+0.7
<u>5.6</u>	<u>5.8</u>	<u>8.1</u>	<u>8.9</u>	<u>8.5</u>	<u>7.2</u>	<u>7.5</u>	<u>8.1</u>	<u>9.2</u>	<u>7.4</u>	<u>6.8</u>
2.5	2.4	1.8	1.5	1.3	3	3	6	8.7	11	2.5

+2.1	+1.6	-1.6	-0.9	0.0	+0.1	-0.6	+1.7	+2.2	+1.7
<u>3.2</u>	<u>3.7</u>	<u>6.9</u>	<u>6.2</u>	<u>5.3</u>	<u>5.2</u>	<u>5.9</u>	<u>3.6</u>	<u>3.1</u>	<u>3.6</u>
2.5	2.5	1.8	1.5	1.4	1.0	1.5	1.8	2.1	2.5

Spike in S.W. side 12' Apple, 60' Lt Cor.

End + 100 ft.

7-21-22 Grades on Curve at
162+87.2

B.M.	0.99	1175.72		1174.73
162+50	with ^{out} fall (Flat)		✓ 2.45	73.27
			2.57	
P.C. 187.2	superelevated .16		✓ 3.42	72.30
163	" .21		✓ 3.20	71.99
+25	" .32		✓ 3.23	71.20
+50	" .42		✓ 3.52	70.31
+75	" .42		✓ 4.20	69.31
164			✓ 5.41	68.26
+25			✓ 7.44	67.21
+50			✓ 8.51	66.16
+75			✓ 8.09	65.11
165		1167.12	✓ 9.56	64.06
+25			✓ 10.61	63.01
+50			✓ 10.19	61.96
+75			✓ 11.60	60.91
166			✓ 11.24	59.86
P.T. +21.06	superelev. .32		✓ 4.15	58.98
+50	" .22		✓ 3.73	57.76
	" .12		✓ 5.20	
			✓ 6.33	
			✓ 5.83	
			✓ 7.20	
			✓ 6.98	
			✓ 4.12	
			✓ 7.16	
			✓ 9.40	
			✓ 9.28	

1175.72
1172.6
1174.6
1173.0
1171.6

722.22
HOT

722.22
300V
300V

51

B.M.	401	1178.74		1174.73
162+50		flat	- 5.47	73.27
162			- 4.94	74.10
+50			- 4.76	74.34
+25			- 4.40	74.21
161			- 4.52	73.94
+50			- 4.52	72.91
160			- 4.92	71.34
+50			- 5.32	69.69
159			- 5.75	68.04
+50			- 7.10	66.39
T.P.	1150	1167.78	- 7.52	1166.28
158			- 7.95	64.74
+50			- 8.17	63.09
157			- 10.20	61.44
+50			- 10.82	59.79
156			- 12.35	58.14
+50			- 12.47	56.49
T.P.	1171	1158.08	- 12.46	1156.37
155	54.76		- 3.04	54.84
+50			- 3.16	53.19
154			- 4.59	51.64
+50			- 4.81	1150.05
T.P.	9.11	1159.16	- 5.34	51.09
+50			- 6.46	51.35
+20			- 7.49	51.77
153			- 7.99	
			- 7.93	
			- 7.22	
			- 7.51	

1159 16

+50			5.19	53.67
			5.21	
152			2.46	56.70
T.P.	9.98	1168 67	2.58	
+50			0.47	1158.69
151			8.72	59.95
+50			5.47	63.20
+50			2.22	66.45
T.P.	12.09	1178.46	2.09	
150			23.0	1166.37
+50			8.75	69.70
149			5.41	72.95
T.P.	10.23	1184.23	5.38	76.12
+50			2.46	1176.00
+25			7.47	78.76
148			6.59	79.85
+50			6.50	80.79
147			5.44	82.20
+50			4.08	83.08
146			4.15	83.87
T.P.	6.58	1191 14	3.87	84.68
+50			2.47	1184.56
145			1.67	85.41
B.M.	3.87	1191.22	5.73	86.00
+50			5.88	1187.35
144			5.16	86.46
+50			5.26	86.78
143			3.87	87.03
			4.76	87.28
			4.44	
			4.86	
			4.10	
			4.51	
			3.74	
			4.16	

1191.22

52

+50			3.96	87.56
142			3.78	87.88
+50			3.39	88.26
141			3.46	88.68
+50			2.96	89.13
T.P.	5.64	1194 62	2.54	1188.90
140			2.66	89.58
+50			2.21	90.03
139			5.04	90.48
+50			7.59	90.93
138			4.77	91.38
T.P.	4.73	1197 38	4.14	1192.65
+50			4.06	92.28
137			3.68	92.73
+50			3.51	93.18
136			3.24	94.08
+50			3.36	94.53
135			1.97	91.83
+50			5.19	92.28
134			5.22	92.73
+50			4.65	93.18
133			4.77	94.08
+50			5.55	94.53
132			5.67	91.83
+50			5.10	92.28
131			5.20	92.73
+50			4.65	93.18
130			4.77	94.08
+50			4.20	94.53
129			4.32	91.83
+50			3.75	92.28
128			3.87	92.73
+50			3.87	93.18
127			3.42	94.08
+50			2.85	94.53
126			2.97	91.83
+50			2.40	92.28
125			2.52	92.73
T.P.	6.54	1201.40	2.57	1194.96

1201, 40

+50		✓	$\frac{5.97}{6.09}$	95.43
133		✓	$\frac{5.52}{5.64}$	95.88
132+50		✓	$\frac{5.97}{5.19}$	96.33
131+90		✓	$\frac{4.53}{4.65}$	96.87
B.M.			4.76	1196.66
+50		✓	$\frac{4.17}{4.29}$	97.23
131		✓	$\frac{3.72}{3.84}$	97.68
+50		✓	$\frac{3.21}{3.33}$	98.19
130		✓	$\frac{2.59}{2.71}$	98.81
+50		✓	$\frac{1.84}{1.96}$	99.56
T.P.	7.90		1.99	1199.41
129		✓	$\frac{6.90}{7.02}$	00.41
+50		✓	$\frac{5.98}{6.10}$	01.33
128		✓	$\frac{5.97}{5.19}$	02.24
+50		✓	$\frac{4.15}{4.27}$	03.16
127		✓	$\frac{3.24}{3.36}$	04.07
+50		✓	$\frac{2.32}{2.44}$	04.99
126		✓	$\frac{1.71}{1.83}$	05.90
T.P.	6.24		1.53	1205.78
+50		✓	$\frac{5.22}{5.34}$	06.82
125		✓	$\frac{4.31}{4.43}$	07.73
+50		✓	$\frac{3.39}{3.51}$	08.65
124		✓	$\frac{2.48}{2.60}$	09.56
B.M.			1.17	1210.91
				1210.87

53

B.M.	5.63	1216 54	1210.91
123+50			$\frac{6.06}{6.18}$ 10.48
123			$\frac{5.15}{5.27}$ 11.39
+50			$\frac{4.23}{4.35}$ 12.31
122			$\frac{3.32}{3.44}$ 13.22
+50			$\frac{2.30}{2.42}$ 14.24
121			$\frac{1.93}{2.05}$ 15.46
T.P.	9.34	1224 68	1.20 1215.34
+50			$\frac{7.80}{7.92}$ 16.88
120			$\frac{6.13}{6.25}$ 18.51
+50			$\frac{4.29}{4.41}$ 20.24
119			$\frac{2.71}{2.83}$ 21.97
+50			$\frac{2.93}{3.05}$ 23.70
T.P.	8.05	1231 63	1.10 1223.58
118			$\frac{6.20}{6.32}$ 25.43
+50			$\frac{4.75}{4.87}$ 26.78
117			$\frac{4.27}{4.39}$ 27.34
+50			$\frac{4.07}{4.19}$ 27.54
116			$\frac{3.87}{3.99}$ 27.76
+50			$\frac{3.67}{3.79}$ 27.96
115			$\frac{3.24}{3.36}$ 28.39
T.P.	6.23	1234 33	3.53 1228.10
+50			$\frac{5.04}{5.16}$ 29.29
114			$\frac{3.92}{4.04}$ 30.41
+50			$\frac{2.72}{2.84}$ 31.54
113			$\frac{1.97}{2.09}$ 32.66
+50			$\frac{0.97}{1.09}$ 33.79

T.P.	6.93	1234 33	0.66	1233.67
112			$\frac{5.69}{\checkmark 5.87}$	34.91
+50			$\frac{4.56}{- 4.68}$	34.04
B.M.			3.87	1236.73
111			$\frac{3.44}{\checkmark 3.56}$	37.16
+50			$\frac{2.31}{\checkmark 2.43}$	38.29
110			$\frac{7.19}{\checkmark 7.31}$	39.41
+50			$\frac{0.96}{\checkmark 1.18}$	40.54
T.P.	4.94	1245 45	0.09	1240.51
109			$\frac{3.79}{\checkmark 3.91}$	41.66
B.M.	8.86	1245 59		1236.73
+50			$\frac{2.80}{- 2.92}$	42.79
108			$\frac{11.58}{\checkmark 7.80}$	43.91
T.P.	9.07	1252 86	1.80	1243.79
+50			$\frac{7.82}{\checkmark 7.94}$	45.04
107			$\frac{6.78}{- 6.90}$	46.16
+50			$\frac{5.57}{- 5.69}$	47.29
106			$\frac{4.45}{- 4.57}$	48.41
+50			$\frac{3.18}{\checkmark 3.30}$	49.68
105			$\frac{1.45}{\checkmark 1.57}$	51.21
T.P.	9.88	1261 90	0.84	1252.02
+50			$\frac{8.87}{\checkmark 8.99}$	53.03
104			$\frac{6.78}{\checkmark 6.90}$	55.12
+50			$\frac{3.55}{\checkmark 3.67}$	57.35
103			$\frac{2.92}{- 3.04}$	59.58
+50			$\frac{2.44}{- 2.56}$	61.81
T.P.	8.49	1270 16	0.23	1261.67
B.M.	3.85	1270 18	3.85	1261.67

		1270 18		
102			$\frac{6.19}{\checkmark 6.31}$	64.04
+85				65.04
+50			$\frac{4.40}{\checkmark 4.52}$	65.78
+25			$\frac{3.71}{\checkmark 3.83}$	66.27
101	0.14.22 Hot			
B.M.	3.46	1269 79		66.33
101			$\frac{3.27}{\checkmark 3.39}$	66.82
+75			$\frac{3.28}{\checkmark 3.40}$	66.51
+50			$\frac{3.52}{\checkmark 3.64}$	66.27
+25			$\frac{4.04}{- 4.16}$	65.75
100			$\frac{4.72}{- 4.84}$	65.00
+75			$\frac{5.79}{- 5.91}$	64.00
+50			$\frac{7.04}{\checkmark 7.16}$	62.75
+25			$\frac{8.42}{\checkmark 8.54}$	61.37
99			$\frac{9.72}{\checkmark 9.84}$	60.00
T.P.	2.97	1262 85	9.91	1259.88
+50			$\frac{5.60}{- 5.72}$	57.25
98			$\frac{8.35}{\checkmark 8.47}$	54.50
+50			$\frac{11.12}{- 11.24}$	51.75
T.P.	1.04	1252 68	11.21	1251.64
97			$\frac{3.54}{\checkmark 3.66}$	49.14
+50			$\frac{5.80}{\checkmark 5.92}$	46.79
96			$\frac{6.01}{- 6.13}$	44.72
+50			$\frac{9.77}{- 9.89}$	42.91
95			$\frac{11.33}{\checkmark 11.45}$	41.39
T.P.	0.17	1241 43	11.42	1241.26
+50			$\frac{1.31}{- 1.43}$	40.12

1241 43

94		✓	$\frac{2.43}{2.55}$	39.00
+50		✓	$\frac{3.55}{3.67}$	37.88
93		✓	$\frac{4.98}{4.80}$	34.75
+50		✓	$\frac{5.75}{5.37}$	35.68
92		✓	$\frac{6.74}{6.86}$	34.69
+50		✓	$\frac{7.63}{7.75}$	33.80
91		✓	$\frac{8.52}{8.65}$	33.00
+50		✓	$\frac{9.18}{9.30}$	32.25
T.P.	3.77		9.30	1232.13
90		✓	$\frac{4.40}{4.52}$	31.50
+50		✓	$\frac{5.15}{5.27}$	30.75
89		✓	$\frac{5.90}{6.02}$	30.00
B.M.	2.04		5.40	1230.57
+50		✓	$\frac{3.80}{3.92}$	29.25
88		✓	$\frac{4.13}{4.25}$	28.42
+50		✓	$\frac{5.12}{5.24}$	27.42
87		✓	$\frac{4.30}{4.42}$	26.25
+50		✓	$\frac{4.63}{4.75}$	24.92
86		✓	$\frac{5.13}{5.25}$	23.42
T.P.	0.44		9.26	1223.29
+50		✓	$\frac{1.98}{2.10}$	21.75
85		✓	$\frac{3.52}{3.64}$	20.21
+50		✓	$\frac{4.66}{4.78}$	19.07
84		✓	$\frac{5.52}{5.64}$	18.14
+50		✓	$\frac{5.77}{5.89}$	17.21
83		✓	$\frac{7.45}{7.57}$	16.28

New Grds
20.41
19.17

200 V.C.

1223 73

+50		✓	$\frac{8.38}{8.50}$	15.35
82		✓	$\frac{9.71}{9.83}$	14.42
+50		✓	$\frac{10.74}{10.86}$	13.49
81		✓	$\frac{11.12}{11.24}$	12.56
J.M.			6.83	1216.90
M.W. cor. s. par. Con. N.W.	0.54		5.33	1212.09
80		✓	$\frac{6.86}{6.98}$	10.56
T.P.	1.57		7.90	1209.52
+50		✓	$\frac{1.79}{1.91}$	09.19
79		✓	$\frac{3.33}{3.45}$	07.76
+50		✓	$\frac{4.11}{4.23}$	07.02
78		✓	$\frac{4.44}{4.56}$	06.65
+50		✓	$\frac{4.29}{4.41}$	06.80
77		✓	$\frac{3.65}{3.77}$	07.44
+50		✓	$\frac{2.55}{2.67}$	08.53
76		✓	$\frac{1.46}{1.58}$	09.68
J.M.	1.97		3.67	1216.29
74+50		✓	$\frac{3.66}{3.78}$	12.67
75		✓	$\frac{4.39}{4.51}$	11.93
+50		✓	$\frac{5.15}{5.27}$	10.83
76		✓	$\frac{6.91}{7.03}$	09.68
+50		✓	$\frac{7.76}{7.88}$	08.53
T.P.	2.37		7.80	1210.86
77		✓	$\frac{3.47}{3.59}$	07.44

Note: Grd. is .08 higher than profile Grd. for 8" pavement

8-23-22

1216 57

B.M. 0.96 1215 28 1214.32

T.P. 221 1215 21 3.57 1213.00

74+25		2.60	
74		2.44	12.88
+50	Lowered (0.1)	2.28	13.00
73	" (0.2)	2.37	12.91
+50	" (0.1)	2.71	12.46
72		2.82	11.96
+50		3.32	11.67
71		3.36	11.79
+50		3.61	12.12
		3.65	12.15
		3.79	
		3.53	
		3.16	
		3.20	
		2.80	
		2.87	

+50		2.74	12.50
		2.75	11.71
		3.58	1206.78
		3.37	1206.77
		8.44	1206.78

T.P. 6.24 1218.64 1212.40

B.M. 517 1211 97 1206.78

70		5.98	12.78
+50		5.90	13.11
69		5.53	13.44
+50		5.20	13.77
68		5.24	14.10
+50		4.82	14.43
67		4.81	14.63
+50		4.54	14.56
66		4.58	14.36
+50		4.25	
		4.21	
	0.1	4.01	
	0.2	4.05	
	0.3	4.09	
		4.12	
		4.18	
		4.32	

C2		0.26	16.71
+50		0.20	10.70
61		1.27	09.44
+50		1.31	07.96
60		2.53	06.36
+50		2.57	04.97
		4.91	
		4.05	
		5.61	
		5.65	
		7.00	
		7.04	

T.P. 2.25 1216 57 1214.32

T.P. 977 1205 69 1204.91

+50		4.32	1416
65		2.26	13.96
+50		2.45	13.76
64		2.61	13.56
+50		2.65	13.36
63		2.84	13.04
+50		2.85	
		3.01	
		3.05	
		3.11	
		3.17	
		3.53	
		3.17	

59		7.06	04.01
+50		4.68	03.26
58		7.72	02.51
+50		2.68	01.76
57		2.77	01.01
+50		3.18	00.52
56		3.73	00.56
+50		3.97	01.12
55		4.68	02.21
+50		4.72	03.56
		5.17	
		5.21	
		5.13	
		5.77	
		4.53	
		4.61	
		3.43	
		3.52	
		2.13	
		2.17	

65 +50 0.3 13.96

T.P. 870 1211 73 1203.55

+50		2.84	13.76
64		2.85	13.56
+50		3.01	13.36
63		3.05	13.04
+50		3.11	
		3.17	
		3.53	
		3.17	

54		6.83	04.91
+50		6.52	06.26
53		5.96	07.61
+50		5.51	1207.22
		4.83	1207.18
		4.16	
		4.51	

Lowered 0.1
Lowered 0.1

J.M. 171 1208.93 1207.22

+75 $\frac{0.87}{-988}$ 08.09

+50 $\frac{0.73}{-276}$ 08.21

+25 $\frac{0.97}{-1.01}$ 07.96

52 $\frac{1.63}{-1.27}$ 07.30

+50 $\frac{3.33}{-833}$ 05.64

51 $\frac{4.95}{-4.97}$ 03.98

+50 $\frac{2.51}{-2.65}$ 02.32

50 $\frac{8.27}{-8.37}$ 00.66

T.P. 0.36 1200 98 831 1200.62

+50 $\frac{1.93}{-2.02}$ 99.00

49 $\frac{3.24}{-3.68}$ 97.31

+50 $\frac{5.25}{-3.23}$ 95.73

48 $\frac{6.78}{-6.80}$ 94.22

+50 $\frac{8.67}{-8.81}$ 92.81

47 $\frac{9.48}{-9.52}$ 91.50

+50 $\frac{10.74}{-10.78}$ 90.24

46 $\frac{12.80}{-12.04}$ 88.98

TP $\frac{9.41}{-9.41}$ 1191.57

J.M. 2.18 1161 29 1159.11

32 $\frac{5.78}{-5.82}$ 55.51

+50 $\frac{7.69}{-7.72}$ 53.61

31 $\frac{9.58}{-9.62}$ 51.71

+50 $\frac{11.48}{-11.52}$ 49.81

T.P. 3.26 1152 40 12.15 1149.14

30 $\frac{1.49}{-1.53}$ 47.91

+50 $\frac{2.39}{-2.43}$ 46.01

+28⁸ PT. $\frac{7.68}{-7.22}$ 45.22

(46.10) V.C.

(45.40) V.C.

1152 40

57

29 $\frac{44.50 V.C.}{-43.77 V.C.}$ 8.18 44.30

+75 $\frac{43.77 V.C.}{-43.08 V.C.}$ 8.14 43.60

+50 $\frac{43.08 V.C.}{-42.45 V.C.}$ 8.10 42.97

+25 $\frac{42.45 V.C.}{-10.83}$ 8.07 42.42

28 $\frac{10.83}{-10.58}$ 8.03 41.86

T.P. 2.40 1144 22 10.58 1141.82

+75 $\frac{2.91}{-2.95}$ 2.91 41.31

+50 $\frac{3.18}{-3.52}$ 3.18 40.74

+25 $\frac{4.05}{-4.07}$ 4.05 40.17

27 $\frac{4.78}{-4.82}$ 4.78 39.44

+75 $\frac{5.96}{-5.90}$ 5.96 38.36

880 $\frac{3.81}{-7.11}$ 3.81 1140.41

+50 $\frac{7.11}{-7.15}$ 7.11 37.11

+25 $\frac{8.38}{-8.38}$ 8.38 35.89

B.M. 0.75 1178 89 3.64 1178.14

A1 $\frac{3.64}{-3.18}$ 3.64 75.75

+50 $\frac{4.67}{-4.15}$ 4.67 74.26

40 $\frac{6.19}{-7.21}$ 6.19 72.74

+50 $\frac{7.21}{-7.75}$ 7.21 71.18

39 $\frac{8.30}{-9.34}$ 8.30 69.59

+50 $\frac{10.93}{-10.97}$ 10.93 67.96

38 $\frac{12.59}{-12.63}$ 12.59 66.30

T.P. 1.37 1167 63 12.63 1166.26

+50 $\frac{3.81}{-3.05}$ 3.81 64.62

37 $\frac{4.67}{-4.67}$ 4.67 62.94

+50 $\frac{6.24}{-6.24}$ 6.24 61.43

36 $\frac{6.24}{-6.24}$ 6.24 60.27

+50 59.44

200 V.C.

Present →

B.M. store at Novelty, blue
cross on N.W. Cor. 2nd.
step to store porch.

Elev = 1108.70

1167.63

37	✓	$\frac{7.83}{4.62}$	63.05
+50	✓	$\frac{5.92}{57.20}$	61.71
36	✓	$\frac{7.97}{7.96}$	60.61
+50	✓	$\frac{7.96}{7.96}$	59.72
35	✓	$\frac{8.56}{8.60}$	59.07
+50	✓	$\frac{8.60}{9.02}$	58.65
34	✓	$\frac{9.39}{7.33}$	58.84
B.M.	✓	$\frac{8.52}{9.60}$	59.11
+50	✓	$\frac{9.60}{9.64}$	62.03
33	✓	$\frac{4.91}{7.95}$	57.72
+50	✓	$\frac{10.66}{10.66}$	57.01
32	✓	$\frac{12.12}{7.12}$	55.51

B.M. 415 1182.29 1178.14

41+50	✓	$\frac{5.99}{5.13}$	77.20
42	✓	$\frac{3.67}{3.71}$	78.62
+50	✓	$\frac{2.29}{2.33}$	80.00
43	✓	$\frac{0.94}{0.91}$	81.35
T.P.		1.01	181.28
+50	✓	$\frac{7.07}{7.06}$	82.66
44	✓	$\frac{5.74}{5.70}$	83.94
+50	✓	$\frac{4.48}{4.52}$	85.20

1189.68

56

15		$\frac{3.22}{3.26}$	86.76
+50		$\frac{1.96}{2.00}$	87.72
46		$\frac{0.70}{0.74}$	88.98
T.P. 5.63		0.74	1188.94
B.M. T.P. 11.		3.00	ck. 91.57
+50	✓	$\frac{4.33}{4.37}$	90.24
47	✓	$\frac{3.07}{3.11}$	91.50

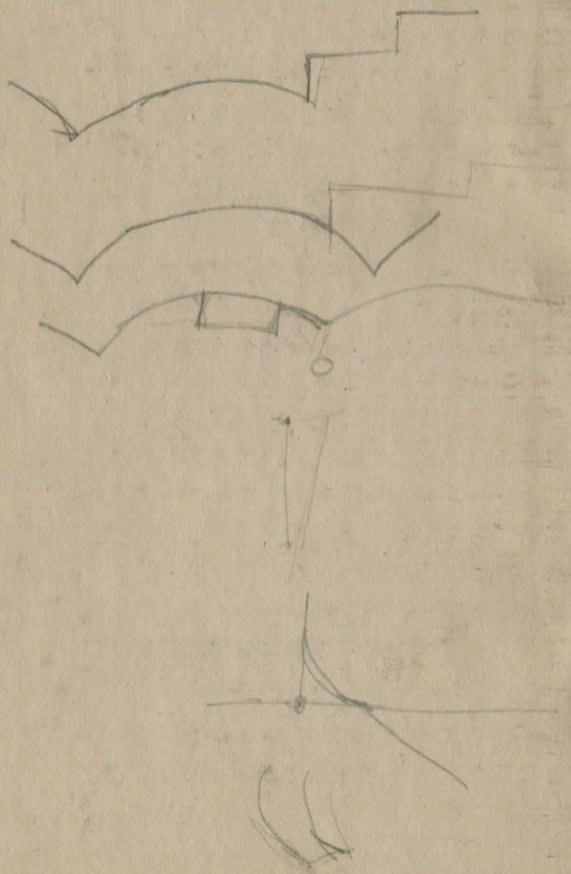
see other level Book

Back part

Geo Walker 154K
 11 - 3rd St
 Willoughby
 4 teams.

16.5
 87.0

102
 10
 105



PLEASE RETURN TO
 CUYAHOGA COUNTY ENGINEER
 COURT HOUSE
 CHARDON, O.
 PHONE 250 X

TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

In.	Dec.	In.	Dec.	In.	Dec.	In.	Dec.	In.	Dec.	In.	Dec.	In.	Dec.
1	.0833	11	.9167	21	.7167	31	.6167	41	.5167	51	.4167	61	.3167
2	.1667	12	.8333	22	.6333	32	.5333	42	.4333	52	.3333	62	.2333
3	.2500	13	.7500	23	.5500	33	.4500	43	.3500	53	.2500	63	.1500
4	.3333	14	.6667	24	.4667	34	.3667	44	.2667	54	.1667	64	.0667
5	.4167	15	.5833	25	.3833	35	.2833	45	.1833	55	.0833	65	.0167
6	.5000	16	.5000	26	.3000	36	.2000	46	.1000	56	.0000	66	
7	.5833	17	.4167	27	.2167	37	.1167	47	.0167	57		67	
8	.6667	18	.3333	28	.1333	38	.0333	48		58		68	
9	.7500	19	.2500	29	.0500	39		49		59		69	
10	.8333	20	.1667	30		40		50		60		70	
11	.9167	30	.0833	40		50		60		70		80	
12	.9167	40	.0167	50		60		70		80		90	
13	.9167	50		60		70		80		90			
14	.9167	60		70		80		90					
15	.9167	70		80		90							
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B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

